GEOTECHNICAL ENGINEERING REPORT

Ann Austin and Hunter Creek Subdivisions

Weil Road Santa Clara, Guadalupe County, Texas

Prepared for:

Lennar San Antonio, Texas

Prepared by: TTL, Inc. San Antonio, Texas

Project No. 00240902004.00 January 22, 2025



17215 Jones Maltsberger Road, Ste. 101 San Antonio, TX 78247 210.888.6100 www.TTLUSA.com

January 22, 2025

Mr. Richard Mott, PE
Director of Land Development
Lennar
1922 Dry Creek Way, Suite 101
San Antonio, TX 78259

O: 210.403.6282

E: Richard.Mott@Lennar.com

RE: Geotechnical Engineering Report

Ann Austin and Hunter Creek Subdivisions

Weil Road

Santa Clara, Guadalupe County, Texas

TTL Project No.00240902004.00

Dear Mr. Mott:

TTL, Inc. (TTL) is pleased to submit this geotechnical engineering report for the above-referenced project. If you have any questions regarding our report, or if additional services are needed, please do not hesitate to contact us.

The enclosed report contains a brief description of the site conditions and our understanding of the project. The preliminary geotechnical recommendations for foundations as well as the final pavement section design recommendations contained within this report are based on our understanding of the proposed development, the results of our field exploration and laboratory tests, and our experience with similar projects.

We appreciate the opportunity to provide these Geotechnical Services for your project and look forward to continuing participation during the design and construction phases of this project.

Respectfully submitted,

TTL, Inc.

Roberto Barajas, PE

Project Professional

Anthony F. Adamo, PE

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GBA Informational Document

APPENDIX A (ILLUSTRATIONS)

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Lab Summary
CBR Plots (CBR-1 thru CBR-4)
Lime Series Curve (CBR-1 and CBR-3)

APPENDIX B (REFERENCE MATERIALS)

Exploration Procedures Laboratory Procedures



1.0 PROJECT INFORMATION

1.1 Project Description

Item	Description	
Project Location	The project site is located on Weil Road approximately one mile southwest of its intersection with N Santa Clara Road in Santa Clara, Guadalupe County, Texas. The Site Location Plan is provided in Appendix A.	
Proposed Development	The project will include the Ann Austin and Hunter Creek Subdivisions. Based on the plat for the Subdivisions, we understand they are adjacent and consist of the following: • Ann Austin – approximately 174 acres with 833 lots • Hunter Creek – approximately 103 acres with 581 lots We understand the subdivision will involve the construction of single-family homes and associated streets.	
Proposed Construction	The geotechnical engineering study will pertain to the design and construction of the streets within the subdivision. The streets are expected to consist of Secondary/Local and Collector streets design as per the City of Santa Clara and Guadalupe design criteria.	
Existing Conditions	Based on Google Earth aerial imagery, the sites appear to have been used as a rural residence and farm. The sites were historically used for agricultural purposes. The outbuildings and water tanks are still in place. Currently much of the land has an overgrowth of vegetation consisting of shrubs and scattered trees. Density of the vegetation varies across the site.	

If the above information is not correct, please contact us so that we can make the necessary modifications to this document and our evaluation and recommendations, if needed.

1.2 Authorization

This Project was authorized by Mr. Richard Mott with Lennar, on August 1, 2024 by acceptance of our Agreement for Services, Nos. P00240902004.00, dated July 16, 2024.

2.0 EXPLORATION FINDINGS

2.1 Site Conditions

The Site consists of approximately 277 acres of land with approximately 1,414 lots across both Subdivisions. Based on Google Earth aerial imagery, the site appears to be a farm with a residence and outbuildings. The land was previously used for agricultural purposes but currently much of the land has overgrowth of vegetation consisting of shrubs and scattered trees. Density of the vegetation varies across the site. A radio tower, multiple structures, and two stock ponds are mapped on the property,

2.2 Site Geology

We reviewed the Geologic Atlas of Texas to determine the geologic setting of the project site and surrounding area. Our review indicated the project site is located within Pecan Gap Chalk (Kpg) of Cretaceous geologic age. This formation generally consists of chalk and chalky marl that weathers into a moderately deep soil. The thickness of this formation generally ranges from 100



to 400 feet. The Pecan Gap Chalk is known to contain expansive clay soils in the area of the project site.

2.3 Subsurface Stratigraphy

Subsurface conditions within the limits of the project were evaluated by drilling forty-six exploratory borings at the approximate locations shown on the Boring Location Plan in Appendix A. **Due to rough terrain access, boring B-39 was not drilled at the time of this report.** Samples obtained during our field exploration were transported to our laboratory where they were reviewed by geotechnical engineering personnel. Representative samples were selected and tested to determine pertinent engineering properties and characteristics for use in our evaluation of the project site. Based on the information developed during our field exploration and laboratory testing, we have determined the stratigraphy of the site is generally as shown on the logs of boring in Appendix A.

The boring logs presented in Appendix A represent our interpretation of the subsurface conditions at each individual boring location. Our interpretation is based on tests and observations performed during drilling operations, visual examination of the soil samples by a geotechnical engineer, and laboratory tests conducted on the retrieved soil samples. The USCS classifications shown on the boring logs represent classifications based on either visual examination, laboratory testing, or both. The lines designating the interfaces between various strata on the boring logs represent the approximate strata boundary. The transition between strata may be more gradual than shown, especially where indicated by a broken line. All data should only be considered accurate at the exact boring locations.

2.4 Subsurface Water Conditions

Subsurface water was not detected either during or upon completion of our exploratory borings. Upon completion of subsurface water observations, the boreholes were backfilled with the spoils generated during drilling operations.

Subsurface water is generally encountered as a 'true' or permanent continuous water source that is generally present year-round or as a discontinuous, isolated "perched" or temporary water source that is temporary. Permanent subsurface water is generally present year-round, which may or may not be influenced by seasonal changes in climate, precipitation, vegetation, surface runoff, water levels in nearby water bodies, and other factors. The subsurface water level below the site may fluctuate up or down in response to such changes and may be at different levels than indicated on the exploration logs at times after the exploration. Temporary subsurface water generally develops as a result of seasonal and climatic conditions.

The Sandy Lean Clay (CL), Sandy Fat Clay (CH), Sandy Silty Clay (CL-ML), Clayey Sand (SC), and Silty Clayey Sand (SC-SM) strata observed at the boring locations are preferential pathways for the transfer of subsurface water. These materials may be present elsewhere at the site and at similar or different depths. The contractor should check for subsurface water before commencement of excavation activities.



3.0 GEOTECHNICAL CONSIDERATIONS

The following geotechnical considerations have been prepared based on the information developed during this Project, our experience with similar projects, and our knowledge of sites with similar surface and subsurface conditions.

3.1 Corrosion Considerations

According to the 2021 IBC, concrete that is exposed to sulfate-containing solutions should be designed in accordance with ACI 318. To evaluate the potential for sulfate exposure, laboratory testing was conducted on material samples recovered during the field exploration to assess the corrosivity risk of the soil at the boring locations. Soil samples were submitted to an analytical lab to determine the sulfate content. The results of the laboratory tests are presented in the following table.

Boring No.	Sample Depth	% Sulfate	ACI 318-19
	(ft.)	by Mass	Exposure Class
B-04	2½ - 4	0.03	S0
B-10	2½ - 4	0.03	S0
B-15	2½ - 4	<0.02	S0
B-19	1/2 -2	0.03	S0
B-25	2½ - 4	0.02	S0
B-28	4½ - 6	0.02	S0
B-34	2½ - 4	0.03	S0
B-37	1/2 - 2	<0.02	S0
B-44	1/2 - 2	<0.02	S0
CBR-1	0 - 2	<0.02	S0
CBR-2	0 - 2	<0.02	S0
CBR-3	0 - 2	<0.02	S0
CBR-4	0 - 2	<0.02	S0

The sulfate test results indicate that the sulfate exposure level across the site is Class S0, which infers that sulfate exposure to lime treatment or concrete is not an issue.

4.0 EARTHWORK RECOMMENDATIONS

4.1 Subgrade Preparation and Stabilization

The intended performance of earth supported elements such as foundations and utilities are contingent upon following the earthwork recommendations and guidelines outlined in this section. Earthwork activities on the project should be observed and evaluated by TTL personnel. The evaluation of earthwork should include observation and testing of all fill and backfill soils placed at the site, along with subgrade preparation beneath the residential structures, pavements, and other areas to receive fill materials.

Please note that mass grading for the subdivision had not been performed before drilling of TTL exploratory borings at the site.



If possible, site development should be performed during seasonably dry weather (typically May through October), and excavation and site preparation should not be performed during or immediately following periods of heavy precipitation or freezing temperatures. Positive surface drainage should be maintained during grading operations and construction to prevent water from ponding on the surface. Surface water run-off from off-site areas should be diverted around the site using berms or ditches. The surface can be rolled smooth to enhance drainage if precipitation is expected but should then be scarified prior to resuming fill placement operations. Subgrades damaged by construction equipment should be promptly repaired to avoid further degradation in adjacent areas and water ponding. Our geoprofessional should provide recommendations for treatment if the subgrade materials become wet, dry, or frozen. When work activities are interrupted by heavy rainfall, fill operations should not be resumed until the moisture content and density of the previously placed fill materials are as recommended in this report. The following earthwork recommendations must be performed prior to pavement and utility construction.

4.1.1 Stripping

Subgrade preparation should begin with stripping the existing vegetation and any otherwise unsuitable materials from planned construction areas.

- Stripping should extend at least 3 feet (horizontal) beyond the construction limits
 or to the property lines, whichever is less. Due to the tree and brush vegetation at
 the site, the stripping depth may need to be at least 12 to 18 inches to completely
 grub and remove the roots.
- Organic-laden strippings including root masses and loose topsoil should be removed from the site or disposed of at designated on-site areas located outside the limits of current or future development.

4.1.2 Proof-rolling

After stripping and excavating to the design subgrade elevation, the stability of exposed subgrades in areas to receive fill should be evaluated by proof-rolling. The stability of subgrades exposed by cutting to final grades should also be evaluated by proof-rolling.

- Perform proof-rolling with a rubber-tired vehicle having a gross vehicle weight of at least 20 tons (such as a loaded tandem-axle dump truck, or similar size/weight construction equipment).
- Proof-rolling equipment should make multiple closely-spaced overlapping passes in perpendicular directions over the subgrade at a walking pace.
- The subgrade should be relatively smooth and free of wheel ruts, sheepsfoot roller dimples, loose clods of soil, or loose gravel; and the subgrade should not be desiccated, cracked, wet, or frozen.
- A TTL geotechnical engineer or their representative should observe the proofrolling to identify, document, and mark areas of unstable subgrade response, such as pumping, rutting, or shoving, if any.



4.1.3 Subgrade Stabilization

Unstable subgrades should be stabilized as recommended below.

- Undercut soft, weak, and unstable soils by excavating below subgrade level to expose stable soils. The excavated soil can be used to restore the excavation subgrade, provided that the soils are relatively free and clean of deleterious material or materials exceeding 3 inches in maximum dimension. The excavated soil, or imported fill soil, shall be placed in maximum 6-inch compacted lifts. Each lift of soil shall be moisture conditioned between plus or minus ±2 percentage points of the optimum moisture content and compacted to at least 95 percent of the maximum dry density determined in accordance with the Standard compaction effort (ASTM D 698). If undercutting deeper than about 3 feet is needed, contact TTL.
- Soil subgrade areas requiring fill placement should be scarified to a depth of about 8 inches and moisture conditioned between ±2 points of the optimum moisture content. The moisture conditioned subgrade should then be compacted to at least 95 percent of the maximum dry density determined in accordance with ASTM D 698. The subgrade should be moisture conditioned just prior to fill placement so the subgrade maintains its compaction moisture levels and does not dry out.
- On-site soils (general fill), Select Fill or Granular Select Fill soil should be placed to achieve the desired elevation as described in Section 4.2 of this report.

4.1.4 <u>Underground Storage Tanks and Septic Tanks</u>

Underground storage tanks, septic tanks, and any associated piping should be excavated and completely removed. On-site soils (i.e., general fill) or select fill meeting the specifications provided in Section 4.2 of this report should then be placed to the match the desired final grade. It is likely that the excavation required to remove these tanks and piping will result in excavation depths greater than 5 feet. Even with proper compaction, it is likely that fill soils placed within this excavation will experience settlement over time. As a result, residential foundations, pavements, and/or utilities may be adversely affected by that settlement. Once final grades are determined and the tanks and piping are removed, an evaluation should be undertaken to determine the most appropriate approach for backfilling the excavation to ensure that any structures or other facilities constructed over the area perform as intended.

4.1.5 Pond Area

The area of the existing pond should be drained (if water is present) and the soils within the pond be mucked out down to stable soils. Muck from the pond should be removed from the site or disposed of at designated on-site areas located outside the limits of current or future development. On-site soils (i.e., general fill) or select fill meeting the specifications provided in Section 4.2 of this report should then be placed to the match the desired final grade. It is likely that the



excavation required to reach stable soils will result in excavation depths greater than 5 feet. Even with proper compaction, it is likely that fill soils placed within this excavation will experience settlement over time. As a result, residential foundations, pavements, and/or utilities may be adversely affected by that settlement. Once final grades are determined and the pond is mucked out, an evaluation should be undertaken to determine the most appropriate approach for backfilling the excavation to ensure that any structures or other facilities constructed over the area perform as intended.

4.2 Compacted Fill Materials

Compacted fill materials may consist of general or select fill depending upon its intended use. The general fill material may consist of onsite soils or select fill materials. General fill material should possess good compaction characteristics that will provide uniform support for pavements or other facilities not extremely sensitive to moments. Select fill materials are typically selected for specific engineering characteristics and performance criteria. These characteristics and criteria are typically dependent on the requirements of the structures or other facilities they are intended to support.

General and select fill materials should be clean and free of any vegetation, roots, organic materials, trash or garbage, construction debris, or other deleterious materials. These materials should contain stones no larger than 3 inches in maximum dimension. The following table provides more specific requirements for general and select fill materials.

Material Type	Characteristics	Compaction Procedures	Compaction Control
GENERAL FILL	Shall consist of CH, CL, SC, GC, SW, or GW as defined by ASTM D 2487. Plasticity Index: Not more than 35. Maximum allowable organic content: 3 percent by weight. This fill material type shall not be used in areas where select fill materials are specified. It is not the intent of this material to control differential soil movements and it shall not be used in areas where control of soil movements is required.	Maximum loose lift thickness: 8 inches. Compaction requirement: Compaction should be at least 95 percent of the standard Proctor (ASTM D 698) maximum dry density for fill bodies less than 5 feet in thickness. Compaction should be at least 95 percent of the modified Proctor (ASTM D 1557) maximum dry density for fill bodies 5 feet or greater in thickness. Moisture content at time of compaction: within plus to minus 3 percent of the material's optimum moisture content.	General Fill Areas: One field test for every 10,000 square feet per lift, with a minimum of two tests per lift. Utility Trenches (in areas where Select Fill is not required): One field density test per every 100 linear feet, per lift.

Material	Characteristics	Compaction	Compaction Control
Туре	Citatacteristics	Procedures	1, 2
	Maximum particle size: 3 inches. Maximum gravel and oversize particle content: 15 percent retained on a ¾-inch sieve. At least 70 percent of total material (by weight) passing the No. 200 sieve	Maximum loose lift thickness: 8 inches with compacted thickness of about 6 inches. Compaction requirement: Compaction should be to at	Building Area: One field density test every 5,000 square feet per lift, with a minimum of two tests per lift. Payement Areas and
SELECT LEAN CLAY FILL (COMPACTED FILL)	Maximum allowable organic content: 3 percent by weight, but large roots are not allowed. Liquid Limit: Not more than 40.	least 95 percent of the standard Proctor maximum (ASTM D 698) dry density for non-roadway areas and TEX-114-E for roadway areas.	Slopes: One field density test every 10,000 square feet per lift, with a minimum of two tests per lift. Utility Trenches: One field
	Plasticity Index: Between 8 and 15. Designation as a CL in accordance with the Unified Soil Classification System (USCS).	Moisture content at time of compaction: within minus 2 to plus 3 percent of the material's optimum moisture content.	density test per structure or one test per every 100 linear feet, per lift.
SELECT GRANULAR FILL (COMPACTED FILL)	Crushed stone (limestone) meeting Type A, Grades 1, 2, or 3; Crushed or uncrushed gravel meeting Type B, Grades 1, 2, or 3; Crushed concrete meeting Type D, Grades 1, 2, or 3; of the 2014 TxDOT Standard Specifications for Construction and Maintenance of Highways, Streets, and Bridges. Designation as a GC or GM in accordance with the USCS Clayey gravel (may locally be referred to as "pitrun" material) or caliche having no particle sizes greater than 3 inches in any dimension, at least 50 percent of total material retained on the No. 200 sieve, a Liquid Limit (LL) no greater than 40, and a PI between 7 and 20. Designation as a GC in accordance with the USCS. Commercial Grade Base (may locally be referred to as "three-quarters to dust" material) that is produced by some local/regional quarries having nothing retained on the 2 inch sieve, at least 60 percent retained on the No. 200 sieve, an LL no greater than 30, and a PI of 7 or less. Designation as a GM in accordance with the USCS.	Maximum loose lift thickness: 8 inches. Compaction requirement: Compaction should be to at least 98 percent of the TEX-113-E dry density. Moisture content at time of compaction: within minus 2 to plus 3 percent of the material's optimum moisture content.	Building Area: One field density test every 5,000 square feet per lift, with a minimum of two tests per lift. Pavement Areas and Slopes: One field density test every 10,000 square feet per lift, with a minimum of two tests per lift. Utility Trenches: One field density test per structure or one test per every 100 linear feet, per lift.

¹For preliminary planning only. Our technician/engineer should determine the actual test frequency.

If grading occurs during wet, cool weather, when drying soils is more difficult and time-consuming, the grading contractor may have difficulty achieving suitable moisture conditions for proper compaction of soil fill.

The surface of any filled area can experience settlement due to compression of the underlying soils, and sometimes additional settlement results from consolidation of thick soil fills due to their own self-weight. For this project, we expect settlements of fills will occur over the course of several years after completion of fill placement due to the nature of the on-site soils. If thicker fills are constructed, settlements could continue for longer periods of time after completion of fill placement, which could adversely affect utilities, structures, or pavements supported by the fill.



² In addition, the fill must be stable under the influence of compaction equipment. Heavy construction traffic should not be allowed to travel on compacted fill areas, except on designated haul roads, to reduce the potential for damaging a previously compacted fill subgrade

4.3 Excavation Conditions

4.3.1 Temporary Slopes and OSHA Soil Types

The Occupational Safety and Health Administration (OSHA) Safety and Health Standards (29 CFR Part 1926) require that excavations be constructed in accordance with the current OSHA guidelines. The contractor is **solely** responsible for designing and constructing stable, temporary excavations and should shore, slope, or bench the sides of the excavations as required to maintain stability of both the excavation sides and bottom. To that end, the contractor's 'responsible person' as defined in 29 CFR Part 1926 should evaluate the required excavations and the soils exposed by those excavations and determine appropriate means as part of the contractor's safety procedures.

OSHA requires that excavations in excess of 5 feet be shored or appropriately sloped. Currently available and practiced methods for achieving excavation stability include sloping, benching, shoring, and the use of trench shields. In excavations that are less than 20 feet deep, OSHA addresses maximum allowable slopes on the Table reproduced below.

Soil or Rock Type	Maximum Allowable Slopes (H:V) ¹ for Excavations Less Than 20 Feet Deep ²	
Stable Rock	Vertical	90°
Type A ³	3⁄4:1	53°
Type B	1:1	45°
Type C	1½:1	34°

- 1. Numbers shown in parentheses next to maximum allowable slopes are angles expressed in degrees from the horizontal. Angles have been rounded off.
- 2. Slopes or benching for excavations that exceed 20 feet shall be designed by a licensed professional engineer.
- 3. For Type A soils, a short-term maximum allowable slope of ½:1 (63°) is allowed in excavations that are 12 feet deep or less. For excavations deeper than 12 feet, the short-term allowable slope shown above applies. OSHA defines short-term as a period of 24 hours or less.

Based on the results of our field and laboratory testing, it is our opinion that the FAT CLAY (CH) and LEAN CLAY (CL) soils encountered in our soil borings may be considered as Type B soils. If those clay soils become saturated or submerged, they should be downgraded to Type C soils. The SANDY FAT CLAY (CH), SANDY LEAN CLAY (CL), SANDY SILTY CLAY(CL-ML), CLAYEY SAND (SC) and SILTY CLAYEY SAND (SC-SM) soils encountered in our soil borings may be considered as Type C soils. We have provided this information solely as a service to our client. The actual OSHA regulations should be consulted prior to any excavations that would be subject to OSHA regulations. TTL does not assume responsibility for any construction site safety or the contractor's or other parties' compliance with local, state, and federal safety or other regulations.

4.3.2 Anticipated Excavation Conditions

The near-surface soils observed at the boring locations are generally Fat Clay and Lean Clay soils. These materials have a firm to hard consistency. The soils encountered at the borings can generally be excavated by conventional earthmoving equipment.



4.3.3 <u>Drainage During Construction</u>

Water should not be allowed to collect in foundation excavations, on foundation surfaces, or on prepared subgrades within the construction area during construction. Excavated areas should be sloped toward designated drainage points to facilitate removal of any collected rainwater, subsurface water, or surface runoff. Positive surface drainage at the site should be provided to reduce infiltration of surface water into subgrades and fill bodies during construction and promote prompt removal of water from the project site.

4.4 Long-Term Drainage Considerations

4.4.1 General

Long-term drainage conditions can have a significant impact on the performance of structures, pavements, utilities, and other ancillary facilities on a project site. We recommend that site drainage be developed such that long-term ponding does not occur except in areas specifically designed for such purposes. When establishing final grades, the design team should be reminded that in expansive clay environments, it is common for ground surface movements to occur that could potentially cause reversal of site drainage patterns and unwanted ponding of surface water. We recommend the following be considered:

- Elevation of the ground surface adjacent to foundations should be at least 6 inches below the Finished Floor Elevation unless measures are taken to ensure long-term positive drainage away from the structures.
- The slope of the ground surface away from the structure (if not covered with pavement) should be a minimum of 5 percent for a distance of at least 10 feet unless measures are taken to ensure long-term positive drainage away from the structure.
- Gutter downspouts should extend at least 5 feet past the edge of the foundations.
- Sufficient slope of the ground surface should be maintained around pavements and other ancillary facilities to ensure long-term positive drainage.

4.4.2 French Drains

Based on the lot layout, it is likely the flow lines of the existing topography will affect the potential for future subsurface water issues. In addition, transient wet weather springs are common in the Cibolo area. These springs may be relatively small in area and based on the 4-inch diameter of the geotechnical borings are often not detected in the Geotechnical subsurface exploration. We understand the site has a fall of about 50 feet across the site which may require a series of tiered French drains. If requested, TTL can provide a cost estimate to provide recommendations for French drains. At a minimum, the Civil Engineer should be made aware of the potential for wet weather springs and give consideration to the use of French Drains at this site.



5.0 INFRASTRUCTURE RECOMMENDATIONS

5.1 Landscape Considerations

We realize landscaping is vital to the aesthetics of any project and is generally typical for residential construction. The owner and design team should be made aware that placing large bushes and trees adjacent to the structures and pavements may contribute to future distress. Vegetation placed in landscape beds adjacent to the structure should be limited to plants and shrubs that will not exceed a mature height of about 3 to 4 feet. Large bushes and trees that will generally exceed these heights should be planted at a reasonable distance away from structures and pavements so their canopy or "drip line" does not extend over the structure when the tree reaches maturity.

Watering of vegetation should be performed in a timely and controlled manner and in sufficient quantity to maintain healthy vegetative cover. Excessive watering should be avoided as excessive irrigation of landscaped areas adjacent to, near or up gradient from foundations and pavements can lead to water migration into building pads and base sections. This migration could cause moisture fluctuations in the underlying clay subgrade which could result in excessive soil movements and loss of subgrade strength.

5.2 Pavement Design Considerations

Based on the American Association of State Highway and Transportation Officials (AASHTO) design guidelines, Guadalupe County Subdivision Regulations, City of Santa Clara Property Subdivision and Land Development Ordinance, and 2013 City of Cibolo Street Pavement Standards, the following design parameters were used for design of the pavement sections:

Acceptable Pavement Structural Sections			
	Marginal	Secondary	Primary
	Access/Minor Street	Collector	Collector
Reliability, %	70	90	90
Initial Serviceability Index, po	4.2	4.2	4.2
Terminal Serviceability Index, pt	2.0	2.5	2.5
Standard Deviation, So	0.45	0.45	0.45
Design Life, years	20	20	20
18-kip ESALs	500,000	1,000,000	2,000,000

Two soil bulk samples were collected to determine the California Bearing Ratio (CBR) value to be used for our pavement design recommendations. The locations at which the CBR bulk samples were taken are indicated on the Boring Location Plan in Appendix A. We performed CBR tests at three compaction levels (i.e. 90%, 95% and 100%) for a total of four CBR tests. Based on laboratory test results, CBR values of 5.3, 3.3, 4.1 and 4.5 percent were obtained for the existing untreated subgrade compacted to at least 95 percent of the maximum dry density determined according to ASTM D 698. The CBR test locations are shown on Exhibit 2, Boring Location Plan. Based on these observations and our experience in the area, TTL Recommends that a CBR value



of 3.0 percent represent the pavement subgrade conditions at this site. There are a number of published correlations relating CBR to the Resilient Modulus (MR). In accordance with the COSA and Bexar County design guidelines, we used a Resilient Modulus (MR) = 1,500 times the CBR in psi, to convert CBR to MR.

Lime Series testing was performed on bulk samples collected for this project. Based on the results of the tests; we anticipate that 5 percent lime (by weight) will be required for this project to obtain a pH of 12.4.

5.2.1 <u>Flexible Pavement Section Recommendations</u>

Following are the recommended flexible pavement sections for Marginal Access/Minor Access, Secondary Collector and Primary Collector.

Flexible Pavement System -		
	Marginal Access/Minor Access	
Component	Pavement Material Thickness, inches	
Hot Mixed Asphaltic Concrete	2½ inches	
Prime Coat	Yes	
Granular Base Course (Type A, Grade 1 or 2)	12 inches	
Lime Treated Subgrade	6 inches	
Required Structural Number	3.18	
Provided Structural Number	3.26	
Required ESALs	500,000	
Provided ESALs	590,576	

Flexible Pavement System		
Commont	Secondary Collector	
Component	Pavement Material Thickness, inches	
Hot Mixed Asphaltic Concrete	3 inches	
Prime Coat	Yes	
Granular Base Course (Type A, Grade 1 or 2)	17½ inches	
Lime Treated Subgrade	6 inches	
Required Structural Number	4.20	
Provided Structural Number	4.25	
Required ESALs	1,000,000	



Flexible Pavement System		
	Secondary Collector	
Component	Pavement Material Thickness, inches	
Provided ESALs	1,082,627	

Flexible Pavement System		
Camananat	Primary Collector	
Component	Pavement Material Thickness, inches	
Hot Mixed Asphaltic Concrete	4 inches	
Prime Coat	Yes	
Granular Base Course (Type A, Grade 1 or 2)	17½ inches	
Lime Treated Subgrade	6 inches	
Required Structural Number	4.67	
Provided Structural Number	4.69	
Required ESALs	2,000,000	
Provided ESALs	2,082,655	

5.2.2 General Guidelines for Pavements

Pavement design methods are intended to provide structural sections with adequate thickness over a particular subgrade such that wheel loads are reduced to a level the subgrade can support. The support characteristics of the subgrade for pavement design do not account for shrink/swell movements of an expansive clayey subgrade. Thus, the pavement may be adequate from a structural standpoint, yet still experience cracking and deformation due to shrink/swell related movement of the subgrade. It is, therefore, important to minimize moisture changes in the subgrade to reduce shrink/swell movements.

On most projects, rough site grading is accomplished relatively early in the construction phase. However, as construction proceeds, excavations are made into these areas; dry weather may desiccate some areas if clay soil is exposed during excavations; rainfall and surface water saturate some areas; heavy traffic from concrete and other delivery vehicles disturbs the subgrade; and many surface irregularities are filled in with loose soils to improve trafficability temporarily. As a result, the pavement subgrade should be carefully evaluated as the time for pavement construction approaches. This is particularly important in and around utility trench cuts.

Thorough proof-rolling of pavement areas using appropriate construction equipment weighing at least 20 tons should be performed no more than 24 hours prior to surface paving. Any problematic areas should be reworked and compacted at that time.



Long-term pavement performance will be dependent upon several factors, including maintaining subgrade moisture levels and providing for preventive maintenance. The following recommendations should be considered at a minimum:

- Maintain and promote proper surface drainage away from pavement edges;
- Consider appropriate edge drainage systems
- Install drainage in areas anticipated for frequent wetting (e.g. landscape beds, discharge area, collection areas, etc.)
- Place joint sealant and seal cracks immediately
- Seal all landscaped areas in, or adjacent to pavements, to minimize or prevent moisture migration to subgrade soils
- Placing compacted, low permeability backfill against the exterior side of curb and gutter
- Extending the base of the curb and gutter system through the pavement base material and at least 6 inches into lime treated subgrade soils

Preventive maintenance should be planned and provided for through an on-going pavement management program. These activities are intended to slow the rate of pavement deterioration and to preserve the pavement investment. This consists of both localized maintenance (e.g. crack and joint sealing and patching) and global maintenance (e.g. surface sealing). Preventive maintenance is usually the first priority when implementing a planned pavement maintenance program and provides the highest return on investment for pavements. Prior to implementing any maintenance, additional engineering observation is recommended to determine the type and extent of preventive maintenance.

5.2.3 Pavement Section Materials

All pavement materials shall conform to the latest edition of the Guadalupe County Subdivision Regulations and the City of Santa Clara Property Subdivision and Land Development Ordinance guidelines unless otherwise approved by the City Engineer. Presented below are selection and preparation guidelines for various materials that may be used to construct the pavement sections. Submittals should be made for each pavement material. The submittals should be reviewed by TTL and any appropriate members of the Project Team. The submittals should provide test information necessary to verify full compliance with the recommended or specified material properties.

Hot Mix Asphaltic Concrete Surface - The paving mixture and construction methods shall conform to Item 340, "Hot Mix Asphaltic Concrete, Type D" of the Standard Specifications by TxDOT. The mix should be compacted between 91 and 95 percent of the maximum theoretical density as measured by TEX-227-F. The asphalt cement content by percent of total mixture weight should fall within a tolerance of ± 0.3 percent asphalt cement from the specific mix. In addition, the mix should be designed so 75 to 85 percent of the voids



in the mineral aggregate (VMA) are filled with asphalt cement. The asphalt cement grades should conform to the following table.

Asphalt Cement Grades										
	Minimum PG Asph									
Street Classifications	Surface Courses	Binder and Level	Base Courses							
	Carrage Courses	up courses	Ducc Courses							
Secondary and Primary Collectors	PG 70-22	PG 70-22	PG 64-22							
Marginal/Minor Access	1 0 70-22	PG 64-22	PG 04-22							

Aggregates known to be prone to stripping should not be used in the hot mix. If such aggregates are used measures should be taken to mitigate this concern. The mix should have at least 70 percent strength retention when tested in accordance with TEX-531-C.

Pavement specimens, which shall be either cores or sections of asphaltic pavement, will be tested according to Test Method TEX-207-F. The nuclear-density gauge or other methods which correlate satisfactorily with results obtained from Project pavement specimens may be used when approved by the Engineer. Unless otherwise shown on the plans, the Contractor shall be responsible for obtaining the required pavement specimens at their expense and in a manner and at locations selected by the Engineer.

<u>Prime Coat</u> - The prime coat should consist of sealing the base with an oil such as MC-30 or AE-P asphalt cement. The prime coat should be applied at a rate not to exceed 0.35 gallons per square yard with materials which meet TxDOT Item 300. The prime coat will help to minimize penetration of rainfall and other moisture that penetrates the base.

<u>Granular Base Material</u> - Base material may be composed of crushed limestone base meeting all of the requirements of 2014 TxDOT Item 247, Type A, Grade 1 or 2; and should have no more than 15 percent of the material passing the No. 200 sieve. The base should be compacted to at least 95 percent of the maximum dry density determined in accordance with test method TEX-113-E at moisture contents ranging between -2 and +3 percentage points of the optimum moisture content.

<u>Lime Treatment</u> - Lime treatment shall be performed only on the dark brown clay subgrade. The subgrade shall be treated with hydrated lime in accordance with TxDOT Item 260. We anticipate that approximately 5 percent hydrated lime will be required (approximately 24 pounds per square yard). The optimum hydrated lime content should result in a soil-lime mixture with a pH of at least 12.4 when tested in accordance with ASTM C 977, Appendix XI.

The hydrated lime should initially be blended with a mixing device such as a pulvermixer. After sufficient moisture conditioning, the treated soil mixture shall be compacted to at least 95 percent of the maximum dry density as determined in accordance with the Standard effort (ASTM D 698) at moisture contents from optimum to +4 percentage points



of the optimum moisture content. If the in-place gradation requirements can be achieved during initial mixing, the remixing after the curing period can be eliminated.

Details regarding subgrade preparation are presented in the Pavement Earthwork Section below.

5.2.4 Pavement Earthwork

The intended performance of street is contingent upon following the earthwork recommendations and guidelines outlined in this section. Earthwork activities on the Project should be observed and evaluated by *TTL* personnel. The evaluation of earthwork should include observation and testing of all fill and backfill soils placed at the Site, subgrade preparation beneath the streets.

The following earthwork recommendations must be performed prior to pavement construction.

- Strip vegetation, loose topsoil, existing pavements, vegetation and any otherwise unsuitable materials from the pavement area. The pavement area is defined as the area that extends at least 3 feet (horizontal) beyond the perimeter of the proposed pavement and any adjacent flatwork (sidewalks).
- Perform cut and fill to accommodate the design pavement subgrade elevation (also referenced as the bottom of the base course). On-site soils can be used for grade adjustments in fill areas. Refer to the Section 4.2 of this draft report for requirements for the placement of on-site soils and select fill materials.
- After achieving the required excavation depth, and before placing any fill, the exposed excavation subgrade should be proof-rolled with at least a 20-ton roller, or equivalent equipment, to evidence any weak yielding zones. A technical representative of our firm should be present to observe the proof-rolling operations. If any weak yielding zones are present, they should be over-excavated, both vertically and horizontally, until competent soils are exposed. The excavated soil can be used to restore the excavation subgrade, provided that the soils are relatively free and clean of deleterious material or materials exceeding 3 inches in maximum dimension. The excavated soil or imported fill soil shall be placed in maximum 6-inch compacted lifts. Each lift of soil shall be moisture conditioned and compacted as described in the Section 4.2 of this draft report.
- Before placing the granular base course, the subgrade soils shall be lime treated. When subgrade soils are stabilized the minimum depth of stabilization shall be 6 inches unless otherwise approved by the City Engineer.
- The lime shall be applied to the subgrade in slurry form unless otherwise approved by the City Engineer. We anticipate that approximately 5 percent of hydrated lime will be required (approximately 24 pounds per square yard). The optimum hydrated lime content should result in a soil-lime mixture with a pH of at least 12.4 when tested in accordance with ASTM C 977, Appendix XI. The hydrated lime should initially be blended with a mixing device such as a pulvermixer. After sufficient moisture conditioning, the treated soil mixture shall be compacted to at least 95 percent of the maximum dry density as determined in accordance with the Standard effort (ASTM D 698) at moisture contents from optimum to +4 percentage points of the optimum moisture content. If the in-place



gradation requirements can be achieved during initial mixing, the remixing after the curing period can be eliminated.

6.0 LIMITATIONS

This geotechnical engineering report has been prepared for the exclusive use of our Client for specific application to this Project. This geotechnical engineering report has been prepared in accordance with generally accepted geotechnical engineering practices using that level of care and skill ordinarily exercised by licensed members of the engineering profession currently practicing under similar conditions in the same locale. No warranties, express or implied, are intended or made.

TTL understands that this geotechnical engineering report will be used by the Client and various individuals and firms' designers and contractors involved with the preliminary design of the Project. TTL should be invited to attend Project meetings (in person or teleconferencing) or be contacted in writing to address applicable issues relating to the geotechnical engineering aspects of the Project. The information provided in this report is intended for planning purposes only and should not be used for final design considerations.

This geotechnical engineering report is based upon the information provided to us by the Client and various other individuals and entities associated with the Project, along with the field exploration, laboratory testing, and engineering analyses and evaluations performed by TTL as described in this report. The Client and readers of this geotechnical engineering report should realize that subsurface variations and anomalies may exist across the site which may not be revealed by our field exploration. Furthermore, the Client and readers should realize that site conditions can change due to the modifying effects of seasonal and climatic conditions and conditions at times after our exploration may be different than reported herein.

The nature and extent of such site or subsurface variations may not become evident until construction commences or is in progress. If site and subsurface anomalies or variations exist or develop, TTL should be contacted immediately so that the situation can be properly evaluated and, if necessary, addressed with provide applicable recommendations.

Unless stated otherwise in this report or in the contract documents between TTL and Client, our scope of services for this Project did not include, either specifically or by implication, any environmental or biological assessment of the site or buildings, or any identification or prevention of pollutants, hazardous materials or conditions at the site or within buildings. If the Client is concerned about the potential for such contamination or pollution, TTL should be contacted to provide a scope of additional services to address the environmental concerns. In addition, TTL is not responsible for permitting, site safety, excavation support, and dewatering requirements.

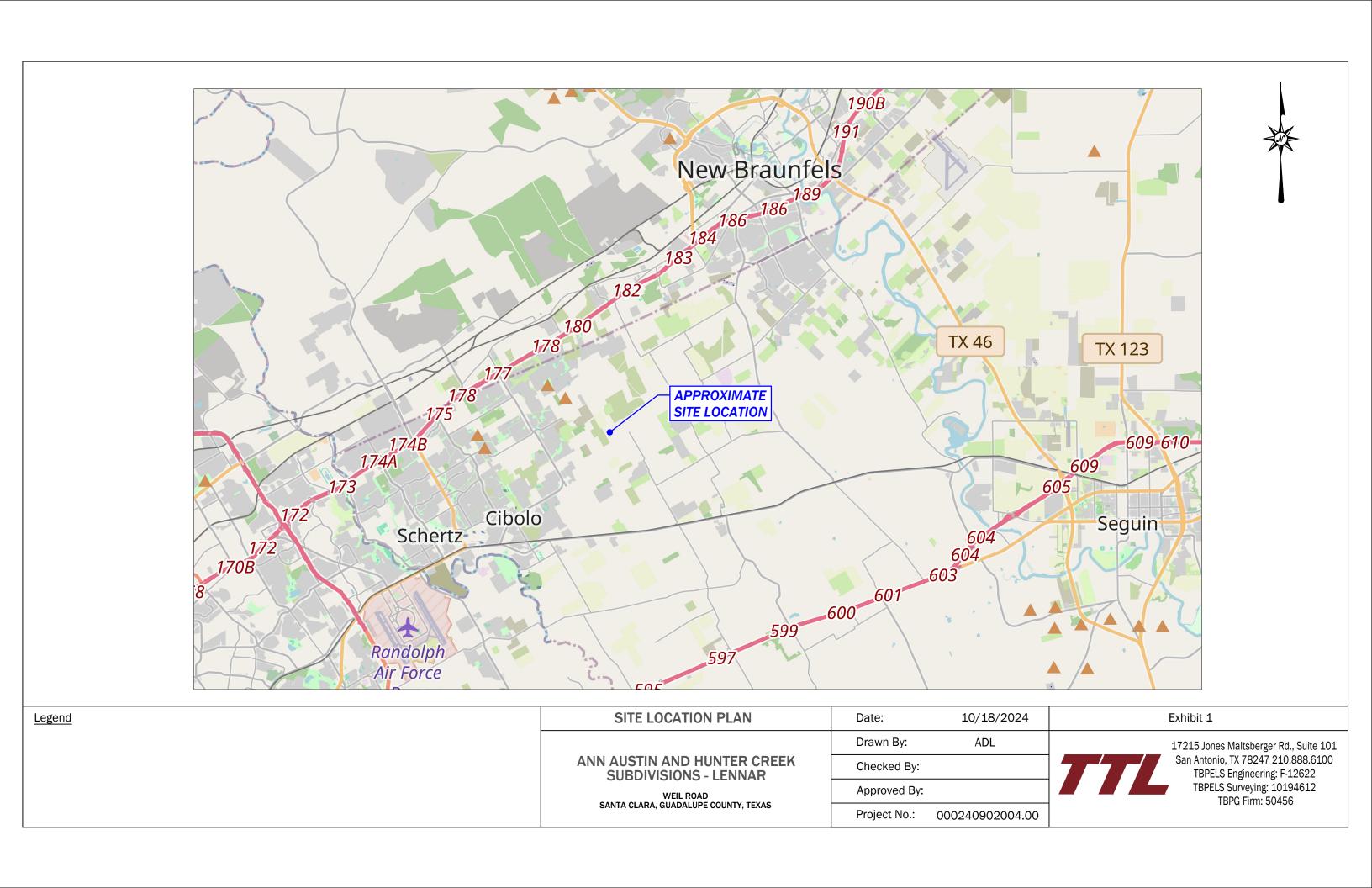
Should the nature, design, or location of the Project, as outlined in this geotechnical engineering report be modified, the geotechnical engineering recommendations and guidelines provided in this document will not be considered valid unless TTL is authorized to review the changes and either verifies or modifies the applicable Project changes in writing.



Additional information about the use and limitations of a geotechnical report is provided within the Geoprofessional Business Association document included at the end of this report.



APPENDIX A ILLUSTRATIONS







Legend Boring Location and Identifier B-X

BORING LOCATION PLAN

ANN AUSTIN AND HUNTER CREEK **SUBDIVISIONS - LENNAR**

WEIL ROAD SANTA CLARA, GUADALUPE COUNTY, TEXAS

10/18/2024 Date: Drawn By: ADL Checked By: Approved By: Project No.: 000240902004.00

17215 Jones Maltsberger Rd., Suite 101 San Antonio, TX 78247 210.888.6100 TBPELS Engineering: F-12622 TBPELS Surveying: 10194612 TBPG Firm: 50456

SOIL LEGEND

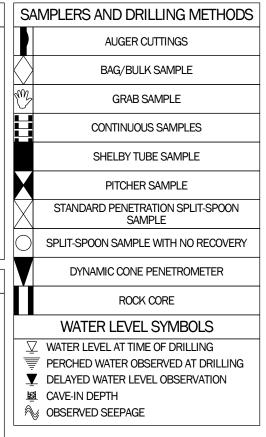
	FINE- AND COARSE-GRAINED SOIL INFORMATION												
FIN	E-GRAINED SO	ILS	COARSE-GI	RAINED SOILS	PARTICLE SIZE								
(SILTS AND CLAYS)			(SANDS AI	ND GRAVELS)	<u>Name</u>	Size (US Std. Sieve)							
SPT N-Value	Consistency	Estimated Q _u (TSF)	SPT N-Value	Relative Density	Boulders	>300 mm (>12 in.)							
0-1	Very Soft	0-0.25	0-4	Very Loose	Cobbles Coarse Gravel	75 mm to 300 mm (3 - 12 in.) 19 mm to 75 mm (3/4 - 3 in.)							
2-4	Soft	0.25 - 0.5	5 - 10	Loose	Fine Gravel	4.75 mm to 19 mm (#4 - 3/4 in.)							
5-8	Firm	0.5 - 1.0	11 - 30	Medium Dense	Coarse Sand	2 mm to 4.75 mm (#10 - #4)							
9-15	Stiff	1.0 - 2.0	31 - 50	Dense	Medium Sand	0.425 mm to 2 mm (#40 - #10)							
16-30	Very Stiff	2.0 - 4.0	51+	Very Dense	Fine Sand	0.075 mm to 0.425 mm							
31+	Hard	4.0+				(#200 - #40)							
Q _u = Uncon	fined Compression	on Strength			Silts and Clays	< 0.075 mm (< #200)							

RELATIVE PROPOF	RTIONS OF SAND AND GRAVEL	RELATIVE PROPORTIONS OF CLAYS AND SILTS						
Descriptive Terms	Percent of Dry Weight	<u>Descriptive Terms</u>	Percent of Dry Weight					
"Trace"	< 15	"Trace"	< 5					
"With"	15 - 30	"With"	5 - 12					
Modifier	> 30	Modifier	> 12					

CRITERIA FO	OR DESCRIBING MOISTURE CONDITION	CRITERIA FOR DESCRIBING CEMENTATION							
<u>Description</u>	Criteria	Description	<u>Criteria</u>						
Dry	Absence of moisture, dusty, dry to the touch	Weak	Crumbles or breaks with handling or little finger pressure						
Moist	Damp, but no visible water	Moderate	Crumbles or breaks with considerable finger pressure						
Wet	Visible free water, usually soil is below water table	Strong	Will not crumble or break with finger pressure						

	CRITERIA FOR DESCRIBING STRUCTURE
<u>Description</u>	<u>Criteria</u>
Stratified	Alternating layers of varying material or color with layers at least 6 mm thick; note the thickness
Laminated	Alternating layers of varying material or color with the layers less than 6 mm thick; note thickness
Fissured	Breaks along definite planes of fracture with little resistance to fracturing
Slickensided	Fracture planes appear polished or glossy, sometimes striated
Blocky	Cohesive soil that can be broken down into small angular lumps which resist further breakdown
Lensed	Inclusion of small pockets of different soils such as small lenses of sand scattered through a mass of clay; note thickness
Homogeneous	Same color and appearance throughout

	ABBREVIATION	IS AND A	ACRONYMS
WOH	Weight of Hammer	N-Value	Sum of the blows for last two 6-in
WOR	Weight of Rod		increments of SPT
Ref.	Refusal	NA	Not Applicable or Not Available
ATD	At Time of Drilling	OD	Outside Diameter
DCP	Dynamic Cone Penetrometer	PPV	Pocket Penetrometer Value
Elev.	Elevation	SFA	Solid Flight Auger
ft.	feet	SH	Shelby Tube Sampler
HSA	Hollow Stem Auger	SS	Split-Spoon Sampler
ID	Inside Diameter	SPT	Standard Penetration Test
in.	inches	USCS	Unified Soil Classification System
Ibs	pounds		





		CLEAN	Cu > 4			SIFICATION SYSTEM (USCS) Well-graded gravels, gravel-sand mixtures with			
	sieve)	GRAVEL WITH	Cc = 1-3		GW	trace or no fines			
	#4	<5% FINES	and/or Cc < 1 Cc > 3		GP	Poorly-graded gravels, gravel-sand mixtures with trace or no fines			
	than th		Cu > 4		GW-GM	Well-graded gravels, gravel-sand mixtures with silt fines			
	is largei	GRAVEL WITH	Cc = 1-3		GW-GC	Well-graded gravels, gravel-sand mixtures with clay fines			
sieve)	raction	5% TO 12% FINES	Cu <u><</u> 4 and/or	2000	GP-GM	Poorly-graded gravels, gravel-sand mixtures with silt fines			
ne #200	coarse i		Cc < 1 Cc > 3		GP-GC	Poorly-graded gravels, gravel-sand mixtures with clay fines			
r than th	50% of			900	GM	Silty gravels, gravel-silt-sand mixtures			
COARSE GRAINED SOILS (>50% of the material is larger than the #200 sieve)	GRAVELS (>50% of coarse fraction is larger than the	MORE	L WITH THAN FINES		GC	Clayey gravels, gravel-sand-clay mixtures			
materia	GR/				GC-GM	Clayey gravels, gravel-sand-clay-silt mixtures			
% of the	ive)	CLEAN SAND WITH	ND Cc = 1-3 trace or no fine			Well-graded sands, sand-gravel mixtures with trace or no fines			
S (>509	e #4 sie	<5% FINES	Cu <u><</u> 6 and/or Cc < 1 Cc > 3		SP	Poorly-graded sands, sand-gravel mixtures with trace or no fines			
JED SOIL	fraction is smaller than the #4 sieve)		Cu > 6		SW-SM	Well-graded sands, sand-gravel mixtures with silt fines			
E GRAIN	smaller	SAND WITH 5% TO	Cc = 1-3		SW-SC	Well-graded sands, sand-gravel mixtures with clay fines			
COARS	action is	12% FINES	Cu <u><</u> 6 and/or		SP-SM	Poorly-graded sands, sand-gravel mixtures with silt fines			
	e)		Cc < 1 Cc > 3		SP-SC	Poorly-graded sands, sand-gravel mixtures with clay fines			
	0% of co				SM	Silty sands, sand-gravel-silt mixtures			
	SANDS (>50% of coars	MORE	WITH THAN FINES		SC	Clayey sands, sand-gravel-clay mixtures			
	SA				SC-SM	Clayey sands, sand-gravel-clay-silt mixtures			
<u>.s</u>		"			ML	Inorganic silts with low plasticity			
naterial	ve)	CLAY!	(Liquid Limit less than 50)		CL	Inorganic clays of low plasticity, gravelly or sandy clays, silty clays, lean clays			
3% of n	200 sie	SILTS & CI	(Liqui less th		CL-ML	Inorganic clay-silts of low plasticity, gravelly clays, sandy clays, silty clays, lean clays			
LS (>5(the #2				OL	Organic silts and organic silty clays of low plasticity			
FINE GRAINED SOILS (>50% of material is	smaller than the #200 sieve	AYS	711(50)		MH	Inorganic silts of high plasticity, elastic silts			
IE GRAII	sma	ILTS & CLAYS	(Liquid Limit nore than 50		СН	Inorganic clays of high plasticity, fat clays			
Z Z		SIL	mo m		ОН	Organic clays and organic silts of high plasticity			

USCS - HIGHLY ORGANIC SOILS Primarily organic matter, dark in color, organic odor Peat, humus, swamp soils with high organic contents

	OTHER MATERIALS
	BITUMINOUS CONCRETE (ASPHALT)
4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	CONCRETE
	CRUSHED STONE/AGGREGATE BASE
77 77 77 77 77 77 77 77 77 77 77 77 77	TOPSOIL
	FILL
	UNDIFFERENTIATED ALLUVIUM
	UNDIFFERENTIATED OVERBURDEN
X	BOULDERS AND COBBLES

$\frac{\text{UNIFORMITY COEFFICIENT}}{C_{\text{u}} = D_{60}/D_{10}}$

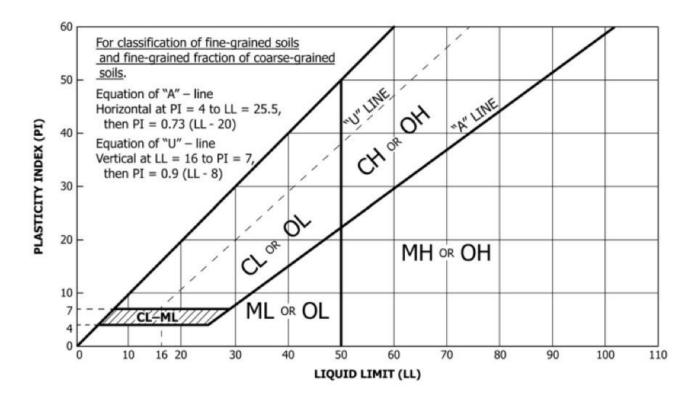
$\frac{\text{COEFFICIENT OF CURVATURE}}{\text{C}_{\text{C}} = (\text{D}_{30})^2/(\text{D}_{60}\text{x}\text{D}_{10})}$

Where:

 D_{60} = grain diameter at 60% passing D_{30} = grain diameter at 30% passing D_{10} = grain diameter at 10% passing



PLASTICITY CHART FOR USCS CLASSIFICATION OF FINE-GRAINED SOILS



IMPORTANT NOTES ON TEST BORING RECORDS

- 1) The report and graphics key are an integral part of these logs. All data and interpretations in this log are subject to the explanations and limitations stated in the report.
- 2) Lines separating strata on the logs represent approximate boundaries only. Actual transitions may be gradual or differ from those shown. Solid lines are used to indicate a change in the material type, particularly a change in the USCS classification. Dashed lines are used to separate two materials that have the same material type, but that differ with respect to two or more other characteristics (e.g. color, consistency).
- 3) No warranty is provided as to the continuity of soil or rock conditions between individual sample locations.
- 4) Logs represent general soil and rock conditions observed at the point of exploration on the date indicated.
- 5) In general, Unified Soil Classification System (USCS) designations presented on the logs were based on visual classification in the field and were modified where appropriate based on gradation and index property testing.
- 6) Fine-grained soils that plot within the hatched area on the Plasticity Chart, and coarse-grained soils with between 5% and 12% passing the #200 sieve require dual USCS symbols as presented on the previous page.
- 7) If the sampler is not able to be driven at least 6 inches, then 50/X" indicates that the sampler advanced X inches when struck 50 times with a 140-pound hammer falling 30 inches.
- 8) If the sampler is driven at least 6 inches, but cannot be driven either of the subsequent two 6-inch increments, then either 50/X'' or the sum of the second 6-inch increment plus 50/X'' for the third 6-inch increment will be indicated.
 - Example 1: Recorded SPT blow counts are 16 50/4", the SPT N-value will be shown as N = 50/4"
 - Example 2: Recorded SPT blow counts are 18 25 50/2", the SPT N-value will be shown as N = 75/8"





Lennar Ann Austin and Hunter Creek Subdivions Weil Road

Log of B-01

					Santa Clara, C	Gudalupe	County	, Texas						Pag	ge 1 of	f 1	
Drillin	g Co.:	TTL,	, Inc.		TTL Project No.:	002409	02004	.00	Rema		vater wa	as not e	ncounte	ered di	ırina dri	llina Th	ne
Driller	r:	T. T.	immer	mann	Date Drilled:	10/10/2	2024		boreh	ole was	backfil	led with	soil cu	ittings	after dri	lling ac	tivities
Logg	ed by:	J. B	arnes		Boring Depth:	10 feet											
Equip	ment:	B-57	7		Boring Elevation:	Ground	l Surfa	се									
Hamr	mer Ty _l	oe: <i>Auto</i>	omatic		Coordinates:	Longit	ude: -9	98.1828 Lati	tude: 2	9.603	86						
Drillin	g Meth	od: Solid	l Flight A	Auger w/SPT Sampling		Γime of Ε	rilling:	Not Encount.	▼ D	elaye	d Wa	ter Le	vel:	N/A			
						of Drillin	g:		Delay	∕ed W	/ater	Obse	rvatio	n Dat	ie:	N/A	
Z O	æ	0								AMF		ATA					
ELEVATION (ft)	DEPTH (ft)	GRAPHIC LOG		MATERIALS	DESCRIPTION	TYPE	N-ATON PROPERTY OF THE PROPERT	N/A DRE/CORE DA 1.6 1.6 9.8 9.1 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1	MOISTURE CONTENT (%)	LIQUID LIMIT	TERBE MITS (S PLASTIC LIMIT PL	RG %) PLASTICITY INDEX	DRY DENSITY (pcf)	SHEAR STRENGTH (psf)	FAILÚRE STRAIN (%)	CONFINING PRESSURE (psi)	% PASSING #200 SIEVE
	- 1 -		FAT	CLAY; stiff to hard, dar trace gravel to 2 feet (k brown to light brown, CH)	with	/	3-4-6 N=10	18								94.7
	- 3 · - 4 ·						<u>/</u>	6 - 8 - 14 N = 22	16								
	- 5 - - 6 ·		- beco	omes calcareous betw	een 4½ and 8 feet		/ \	4 - 14 - 21 N = 35	16	54	18	36					
	- 7 ·		- SAN	NDY FAT CLAY (CH) I	ayer between 6½ and 8	feet	/	21 - 28 - 23 N = 51	10								68.
	– 9 ·					X	/	8 - 13 - 17 N = 30	12	66	19	47					
	- 10 -			Boring termin	ated at 10 feet.												
	- 11 -	1															
	- 12	-															
	40																
	- 13 ·																
	– 14 ·	-															
				om the corresponding Instrume	4.60										01:		Щ.



Lennar Ann Austin and Hunter Creek Subdivions Weil Road

Log of B-02

Santa Clara, Gudalupe County, Texas Page 1 of 1 Remarks: Drilling Co.: TTL, Inc. TTL Project No.: 00240902004.00 Subsurface water was not encountered during drilling. The borehole was backfilled with soil cuttings after drilling activities Driller: T. Timmermann Date Drilled: 10/10/2024 were completed. Logged by: J. Barnes Boring Depth: 10 feet Equipment: B-57 Boring Elevation: Ground Surface Hammer Type: Automatic Coordinates: Longitude: -98.1844 Latitude: 29.6045 Delayed Water Level: N/A Drilling Method: Solid Flight Auger w/SPT Sampling Encount. Cave-In at Time of Drilling: Delayed Water Observation Date: N/A SAMPLE DATA BORE/CORE DATA ELEVATION (ft) DEPTH (ft) GRAPHIC LOG ATTERBERG LIMITS (%) DRY DENSITY (pcf) SHEAR STRENGTH (psf) FAILURE STRAIN (%) MOISTURE CONTENT **MATERIALS DESCRIPTION** 1st 6" 2nd 6" 3rd 6" RQD LIQUID Report: AEP-GEOTECH LOG - LAT LONG % REC N-VALUE BLOWS/FT LL PL ы SANDY LEAN CLAY; stiff, dark brown (CL) 10 - 7 - 4 12 FAT CLAY WITH SAND; very stiff, gray to very dark brown, trace gravel (CH) 20/1/25 6 - 7 - 10 8 19 68 49 N = 17X:2024/09/24-09-02004.00 - LENNAR - ANN AUSTIN/GEOTECHNICAL/DATA\00240902004.00 -- HUNTER CREEK ANN AUSTIN.GPJ - becomes stiff between 41/2 and 6 feet 4-6-6 81.8 18 7 - 9 - 14 23 47 N = 236 - 9 - 16 19 N = 25 10 Boring terminated at 10 feet. 11 12 13 14



14

Lennar **Ann Austin and Hunter Creek Subdivions** Weil Road

Log of **B-03**

Santa Clara, Gudalupe County, Texas Page 1 of 1 Remarks: Drilling Co.: TTL, Inc. TTL Project No.: 00240902004.00 Subsurface water was not encountered during drilling. The borehole was backfilled with soil cuttings after drilling activities Driller: T. Timmermann Date Drilled: 10/10/2024 were completed. Logged by: J. Barnes Boring Depth: 10 feet Equipment: B-57 Boring Elevation: Ground Surface Hammer Type: Automatic Coordinates: Longitude: -98.1838 Latitude: 29.6053 Delayed Water Level: N/A Drilling Method: Solid Flight Auger w/SPT Sampling Encount. Cave-In at Time of Drilling: Delayed Water Observation Date: N/A SAMPLE DATA BORE/CORE DATA ELEVATION (ft) DEPTH (ft) GRAPHIC LOG ATTERBERG LIMITS (%) DRY DENSITY (pcf) SHEAR STRENGTH (psf) FAILURE STRAIN (%) MOISTURE CONTENT **MATERIALS DESCRIPTION** 1st 6" 2nd 6" 3rd 6" RQD LIQUID Report: AEP-GEOTECH LOG - LAT LONG % REC N-VALUE BLOWS/FT LL PL ы SANDY LEAN CLAY; very stiff, dark brown (CL) 3-6-10 10 N = 16 FAT CLAY; very stiff to hard, brownish-gray to dark brown and light brown (CH) 20/1/25 8 - 11 - 15 18 15 64 46 N = 26X:2024/09/24-09-02004.00 - LENNAR - ANN AUSTIN/GEOTECHNICAL/DATA\00240902004.00 -- HUNTER CREEK ANN AUSTIN.GPJ - becomes calcareous between 41/2 and 8 feet 7 - 11 - 13 97.2 13 N = 24 18 - 25 - 14 15 N = 39- becomes light brown and light gray below 81/2 feet 8 - 16 - 19 16 69 19 50 N = 3510 Boring terminated at 10 feet. 11 12 13



Lennar Ann Austin and Hunter Creek Subdivions Weil Road

Log of B-04

Santa Clara, Gudalupe County, Texas Page 1 of 1 Remarks: Drilling Co.: TTL, Inc. TTL Project No.: 00240902004.00 Subsurface water was not encountered during drilling. The borehole was backfilled with soil cuttings after drilling activities Driller: T. Timmermann Date Drilled: 10/10/2024 were completed. Logged by: J. Barnes Boring Depth: 10 feet Equipment: B-57 Boring Elevation: Ground Surface Hammer Type: Automatic Coordinates: Longitude: -98.1845 Latitude: 29.6062 Delayed Water Level: N/A Drilling Method: Solid Flight Auger w/SPT Sampling Encount. Cave-In at Time of Drilling: Delayed Water Observation Date: N/A SAMPLE DATA BORE/CORE DATA ELEVATION (ft) DEPTH (ft) GRAPHIC LOG ATTERBERG LIMITS (%) DRY DENSITY (pcf) SHEAR STRENGTH (psf) FAILURE STRAIN (%) MOISTURE CONTENT **MATERIALS DESCRIPTION** 1st 6" 2nd 6" 3rd 6" RQD LIQUID PLASTIC LIMIT Report: AEP-GEOTECH LOG - LAT LONG % REC N-VALUE BLOWS/FT LL PLы SANDY SILTY CLAY; firm, gray (CL-ML) 1-3-4 11 26 22 4 FAT CLAY; very stiff to hard, gray to brown (CH) 20/1/25 7 - 10 - 14 14 96.6 N = 24X:2024/09/24-09-02004.00 - LENNAR - ANN AUSTIN/GEOTECHNICAL/DATA\00240902004.00 -- HUNTER CREEK ANN AUSTIN.GPJ 6-9-9 47 66 19 14 13 - 18 - 16 18 92.9 N = 34- becomes light brown and light gray below 81/2 feet 6 - 8 - 12 23 N = 20 10 Boring terminated at 10 feet. 11 12 13 14



14

Lennar **Ann Austin and Hunter Creek Subdivions** Weil Road

Log of **B-05**

Santa Clara, Gudalupe County, Texas Page 1 of 1 Remarks: Drilling Co.: TTL, Inc. TTL Project No.: 00240902004.00 Subsurface water was not encountered during drilling. The borehole was backfilled with soil cuttings after drilling activities Driller: T. Timmermann Date Drilled: 10/10/2024 were completed. Logged by: J. Barnes Boring Depth: 10 feet Equipment: B-57 Boring Elevation: Ground Surface Hammer Type: Automatic Coordinates: Longitude: -98.1849 Latitude: 29.6080 Delayed Water Level: N/A Drilling Method: Solid Flight Auger w/SPT Sampling Encount. Cave-In at Time of Drilling: Delayed Water Observation Date: N/A SAMPLE DATA BORE/CORE DATA ELEVATION (ft) DEPTH (ft) GRAPHIC LOG ATTERBERG LIMITS (%) MOISTURE CONTENT **MATERIALS DESCRIPTION** DENSIT 1st 6" 2nd 6" 3rd 6" RQD LIQUID Report: AEP-GEOTECH LOG - LAT LONG % REC N-VALUE BLOWS/FT LL PL ы LEAN CLAY; firm, dark brown (CL) 2-3-3 97.6 17 FAT CLAY; stiff to very stiff, very dark brown to brown (CH) 20/1/25 3-5-8 23 72 21 51 N = 13X:2024/09/24-09-02004.00 - LENNAR - ANN AUSTIN/GEOTECHNICAL/DATA\00240902004.00 -- HUNTER CREEK ANN AUSTIN.GPJ - slightly calcareous between 41/2 and 6 feet 6 - 10 - 12 96.2 21 N = 22 12 - 15 - 14 69 23 46 N = 29becomes light brown and brown between $8\frac{1}{2}$ and 10 5 - 8 - 15 20 N = 23 10 Boring terminated at 10 feet. 11 12 13



X:202409/24-09-02004.00 - LENNAR - ANN AUSTIN/GEOTECHNICAL/DATA\0024092004.00 -- HUNTER CREEK ANN AUSTIN.GFJ

Lennar Ann Austin and Hunter Creek Subdivions Weil Road

Log of B-06

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					Santa Clara, Gudalupe County, Texas					Page 1 of 1							f 1			
Drillin	ıg Co.:	TTL	, Inc.		 Project No.: 00240902004.00					Remarks: Subsurface water was not encountered during drilling. The										
Driller: T. Timmermann					Date Drilled:	10/10	0/2	024			ole was	backfi					illing ac			
Logged by: J. Barnes				Boring Depth:	10 fe	et														
Equip	oment:	B-5	7		Boring Elevation:	Grou	ınd	Surface												
Hammer Type: Automatic				Coordinates:																
Drilling Method: Solid Flight Auger w/SPT Sampling									▼ Delayed Water Level: N/A											
	T					of Dril	lling	g: <i>N/A</i>		Delay	ed W	/ater	Obse	rvatio	n Dat	te:	N/A			
z						SAMPLE DA														
ELEVATION (ft)	DEPTH (ft)	GRAPHIC LOG		MATERIALS	DESCRIPTION		TYPE	BORE/CC	RE DATA	MOISTURE CONTENT (%)	LIQUID LIMIT	TERBE MITS (* PLASTIC LIMIT	%) I	DRY DENSITY (pcf)	SHEAR STRENGTH (psf)	FAILURE STRAIN (%)	CONFINING PRESSURE (psi)	% PASSING #200 SIEVE		
	- 1 -			DY LEAN CLAY; stiff,				3 - 4 - N = 9	5	14										
	- 3 -							7 - 8 - N = 1!		22								91.		



Lennar **Ann Austin and Hunter Creek Subdivions** Weil Road

Log of **B-07**

Santa Clara, Gudalupe County, Texas

Page 1 of 1 Remarks: Drilling Co.: TTL, Inc. TTL Project No.: 00240902004.00 Subsurface water was not encountered during drilling. The borehole was backfilled with soil cuttings after drilling activities Driller: T. Timmermann Date Drilled: 10/10/2024 were completed. Logged by: J. Barnes Boring Depth: 10 feet Equipment: B-57 Boring Elevation: Ground Surface Hammer Type: Automatic Coordinates: Longitude: -98.1867 Latitude: 29.6073 Delayed Water Level: N/A Drilling Method: Solid Flight Auger w/SPT Sampling Encount. Cave-In at Time of Drilling: Delayed Water Observation Date: N/A SAMPLE DATA ELEVATION (ft) DEPTH (ft) GRAPHIC LOG ATTERBERG LIMITS (%) BORE/CORE DATA DRY DENSITY (pcf) SHEAR STRENGTH (psf) FAILURE STRAIN (%) MOISTURE CONTENT **MATERIALS DESCRIPTION** 1st 6" 2nd 6" 3rd 6" RQD LIQUID Report: AEP-GEOTECH LOG - LAT LONG % REC N-VALUE BLOWS/FT LL PL ы LEAN CLAY; very stiff, dark brown (CL) 6-7-9 99.6 13 FAT CLAY; very stiff to hard, dark brown to light brown (CH) 20/1/25 10 - 11 - 16 20 16 50 30 N = 27X:2024/09/24-09-02004.00 - LENNAR - ANN AUSTIN/GEOTECHNICAL/DATA\00240902004.00 -- HUNTER CREEK ANN AUSTIN.GPJ 8 - 14 - 20 93.8 15 8 - 21 - 23 14 63 19 44 N = 44becomes light brown and light gray, calcareous below 8½ feet 9 - 13 - 17 18 N = 3010 Boring terminated at 10 feet. 11 12 13 14



14

Lennar **Ann Austin and Hunter Creek Subdivions** Weil Road

Log of **B-08**

Santa Clara, Gudalupe County, Texas Page 1 of 1 Remarks: Drilling Co.: TTL, Inc. TTL Project No.: 00240902004.00 Subsurface water was not encountered during drilling. The borehole was backfilled with soil cuttings after drilling activities Driller: T. Timmermann Date Drilled: 10/10/2024 were completed. Logged by: J. Barnes Boring Depth: 10 feet Equipment: B-57 Boring Elevation: Ground Surface Hammer Type: Automatic Coordinates: Longitude: -98.1882 Latitude: 29.6063 Delayed Water Level: N/A Drilling Method: Solid Flight Auger w/SPT Sampling Encount. Cave-In at Time of Drilling: Delayed Water Observation Date: N/A SAMPLE DATA BORE/CORE DATA ELEVATION (ft) DEPTH (ft) GRAPHIC LOG ATTERBERG LIMITS (%) DRY DENSITY (pcf) SHEAR STRENGTH (psf) FAILURE STRAIN (%) MOISTURE CONTENT **MATERIALS DESCRIPTION** 1st 6" 2nd 6" 3rd 6" RQD LIQUID Report: AEP-GEOTECH LOG - LAT LONG % REC N-VALUE BLOWS/FT LL PL ы CLAYEY SAND; loose to medium dense, dark brown, trace gravel (SC) 2-4-5 12 2 3 20/1/25 9 - 11 - 17 11 N = 28SANDY LEAN CLAY; hard, pale brown and brown (CL) X:2024\09\24-09-02004.00 - LENNAR - ANN AUSTIN\GEOTECHNICAL\DATA\00240902004.00 -- HUNTER CREEK ANN AUSTIN\GPJ 5 8 - 15 - 17 7 57.1 16 28 44 N = 326 22 - 18 - 23 5 N = 418 FAT CLAY; hard, light brown, calcareous (CH) 11 - 18 - 23 9 53 16 37 88.7 N = 4110 Boring terminated at 10 feet. 11 12 13



Lennar Ann Austin and Hunter Creek Subdivions Weil Road

Log of B-09

Santa Clara, Gudalupe County, Texas Page 1 of 1 Remarks: Drilling Co.: TTL, Inc. TTL Project No.: 00240902004.00 Subsurface water was not encountered during drilling. The borehole was backfilled with soil cuttings after drilling activities Driller: T. Timmermann Date Drilled: 10/10/2024 were completed. Logged by: J. Barnes Boring Depth: 10 feet Equipment: B-57 Boring Elevation: Ground Surface Hammer Type: Automatic Coordinates: Longitude: -98.1876 Latitude: 29.6052 Delayed Water Level: N/A Drilling Method: Solid Flight Auger w/SPT Sampling Encount. Cave-In at Time of Drilling: Delayed Water Observation Date: N/A SAMPLE DATA BORE/CORE DATA ELEVATION (ft) DEPTH (ft) GRAPHIC LOG ATTERBERG LIMITS (%) MOISTURE CONTENT **MATERIALS DESCRIPTION** 1st 6" 2nd 6" DENSIT 3rd 6" RQD LIQUID Report: AEP-GEOTECH LOG - LAT LONG % REC N-VALUE BLOWS/FT LL PL ы LEAN CLAY; stiff, brownish-gray (CL) 5-6-5 10 91.7 FAT CLAY; stiff to hard, dark brown to brownish-gray (CH) 20/1/25 5-6-5 22 48 12 70 N = 11X:2024/09/24-09-02004.00 - LENNAR - ANN AUSTIN/GEOTECHNICAL/DATA\00240902004.00 -- HUNTER CREEK ANN AUSTIN.GPJ 6-8-9 19 8 - 10 - 10 7 89.4 N = 20becomes dark brown and light brown, trace gravel below 81/2 feet 10 - 21 - 21 8 17 35 52 N = 42 10 Boring terminated at 10 feet. 11 12 13 14



Log of **B-10**

Santa Clara, Gudalupe County, Texas

Page 1 of 1

Remarks: Drilling Co.: TTL, Inc. TTL Project No.: 00240902004.00 Subsurface water was not encountered during drilling. The borehole was backfilled with soil cuttings after drilling activities Driller: T. Timmermann Date Drilled: 10/10/2024 were completed. Logged by: J. Barnes Boring Depth: 10 feet Equipment: B-57 Boring Elevation: Ground Surface Hammer Type: Automatic Longitude: -98.1862 Latitude: 29.6042 Coordinates: Delayed Water Level: N/A Drilling Method: Solid Flight Auger w/SPT Sampling Encount. Cave-In at Time of Drilling: Delayed Water Observation Date: N/A SAMPLE DATA BORE/CORE DATA ELEVATION (ft) DEPTH (ft) GRAPHIC LOG ATTERBERG LIMITS (%) MOISTURE CONTENT **MATERIALS DESCRIPTION** 1st 6" 2nd 6" 3rd 6" RQD LIQUID PLASTIC LIMIT Report: AEP-GEOTECH LOG - LAT LONG % REC N-VALUE BLOWS/FT LL PL ы FAT CLAY WITH SAND; stiff, dark brown (CH) 4-4-5 13 67 21 46 FAT CLAY; stiff to very stiff, dark brown (CH) 20/1/25 5-6-8 23 X:2024/09/24-09-02004.00 - LENNAR - ANN AUSTIN/GEOTECHNICAL/DATA\00240902004.00 -- HUNTER CREEK ANN AUSTIN.GPJ 2-4-5 88.0 29 2-5-6 71 50 N = 11becomes light brown and light gray, calcareous below 8½ feet 9 - 10 - 9 15 10 Boring terminated at 10 feet. 11 12 13 14



Log of B-11

Santa Clara, Gudalupe County, Texas Page 1 of 1 Remarks: Drilling Co.: TTL, Inc. TTL Project No.: 00240902004.00 Subsurface water was not encountered during drilling. The borehole was backfilled with soil cuttings after drilling activities Driller: T. Timmermann Date Drilled: 10/10/2024 were completed. Logged by: J. Barnes Boring Depth: 10 feet Equipment: B-57 Boring Elevation: Ground Surface Hammer Type: Automatic Longitude: -98.1852 Latitude: 29.6028 Coordinates: ▼ Delayed Water Level: N/A Drilling Method: Solid Flight Auger w/SPT Sampling Encount. Cave-In at Time of Drilling: Delayed Water Observation Date: N/A SAMPLE DATA BORE/CORE DATA ELEVATION (ft) DEPTH (ft) GRAPHIC LOG ATTERBERG LIMITS (%) DRY DENSITY (pcf) SHEAR STRENGTH (psf) FAILURE STRAIN (%) MOISTURE CONTENT **MATERIALS DESCRIPTION** 1st 6" 2nd 6" 3rd 6" RQD LIQUID Report: AEP-GEOTECH LOG - LAT LONG % REC N-VALUE BLOWS/FT LL PL ы FAT CLAY; stiff to very stiff, dark brown and gray (CH) 4-5-6 92.8 15 20/1/25 7 - 8 - 12 14 N = 20FAT CLAY WITH SAND; stiff to very stiff, dark brown to X:2024/09/24-09-02004.00 - LENNAR - ANN AUSTIN/GEOTECHNICAL/DATA\00240902004.00 -- HUNTER CREEK ANN AUSTIN.GPJ gray (CH) 5-6-7 69 19 50 14 - trace gravel between 61/2 and 8 feet 8 - 10 - 18 16 81.7 N = 288 LEAN CLAY; hard, light brown and light gray (CL) 9 9 - 18 - 24 15 29 13 44 N = 4210 Boring terminated at 10 feet. 11 12 13 14



Log of B-12

Santa Clara, Gudalupe County, Texas

Page 1 of 1

					Santa Clara, G	udalupe	e C	ounty, rexas						Pag	je 1 of	T 1	
Drillin	g Co.:	TTL	., Inc.		TTL Project No.:	00240	90	2004.00	Rema		ater wa	as not e	encount	ered du	ırina dri	llina Ti	he
Driller	r:	Т. Т	īmmei	rmann	Date Drilled:	10/10/	/20	024	boreh	ole was	backfil	led with	n soil ci	uttings a	after dri	lling ac	tivitie
Logg	ed by:	J. B	arnes		Boring Depth:	10 fee	et										
Equip	ment:	B-5	7		Boring Elevation:	Groun	nd .	Surface									
Hamr	mer Ty	pe: <i>Auto</i>	omatic	:	Coordinates:	Longi	itu	de: -98.1866 Latitu	ıde: 2	9.602	9						
Drillin	g Meth	od: Solia	l Flight /	Auger w/SPT Sampling		ime of	Dr	illing: Not Encount.	▼ D	elaye	d Wa	ter Le	evel:	N/A			
						of Drilli	ing		Delay	∕ed W	/ater	Obse	rvatio	n Dat	e:	N/A	
z	t)							-		SAMF							
ELEVATION (ft)	DEPTH (ft)	GRAPHIC LOG		MATERIALS	DESCRIPTION	Ĺ		BORE/CORE DATA 19 19 10 10 10 10 10 10 10 10 10 10 10 10 10	MOISTURE CONTENT (%)	LIQUID	TERBE MITS (9 PLASTIC LIMIT	RG %) PLASTICITY INDEX	DRY DENSITY (pcf)	SHEAR STRENGTH (psf)	FAILURE STRAIN (%)	CONFINING PRESSURE (psi)	% PASSING
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	- 6					1	-\										
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	- 7					\	\bigvee	17 - 22 - 27	12	58	20	38					
						/	$\setminus \mid$	N = 49									
	8					1	_										
			- bec	comes dark brown, brow	wn and gray below 8½ fe	et											
	⊢ 9 					\	\mathbb{V}	19 - 23 - 24 N = 47	15								
	40					/	/\										
				Boring termin	ated at 10 feet.												
	- 11																
	''																
	- 12																
	- 13																
	- 14	-															
Thi	a barina lag	s aball not be a			4.50	-4		oring log or the corresponding l		4 - 4 C					Oliant A		



il Road

Santa Clara, Gudalupe County, Texas

Page 1 of 1

Log of

B-13

Remarks: Drilling Co.: TTL, Inc. TTL Project No.: 00240902004.00 Subsurface water was not encountered during drilling. The borehole was backfilled with soil cuttings after drilling activities Driller: T. Timmermann Date Drilled: 10/10/2024 were completed. Logged by: J. Barnes Boring Depth: 10 feet Equipment: B-57 Boring Elevation: Ground Surface Hammer Type: Automatic Coordinates: Longitude: -98.1876 Latitude: 29.6041 Delayed Water Level: N/A Drilling Method: Solid Flight Auger w/SPT Sampling Encount. Cave-In at Time of Drilling: Delayed Water Observation Date: N/A SAMPLE DATA ELEVATION (ft) DEPTH (ft) GRAPHIC LOG ATTERBERG LIMITS (%) BORE/CORE DATA DRY DENSITY (pcf) SHEAR STRENGTH (psf) FAILURE STRAIN (%) MOISTURE CONTENT **MATERIALS DESCRIPTION** 1st 6" 2nd 6" 3rd 6" RQD LIQUID PLASTIC LIMIT Report: AEP-GEOTECH LOG - LAT LONG % REC N-VALUE BLOWS/FT LL PL ы SANDY LEAN CLAY; firm to stiff, dark brown (CL) 2-3-5 10 2 3 20/1/25 5-6-9 12 N = 15FAT CLAY; very stiff, dark brown and light brown (CH) X:2024/09/24-09-02004.00 - LENNAR - ANN AUSTIN/GEOTECHNICAL/DATA\00240902004.00 -- HUNTER CREEK ANN AUSTIN.GPJ 6 - 10 - 12 96.7 18 N = 22 11 - 10 - 12 16 76 52 N = 2210 - 13 - 15 19 67 18 49 N = 28 10 Boring terminated at 10 feet. 11 12 13 14



12

13

14

Lennar **Ann Austin and Hunter Creek Subdivions** Weil Road

Log of **B-14**

Santa Clara, Gudalupe County, Texas Page 1 of 1 Remarks: Drilling Co.: TTL, Inc. TTL Project No.: 00240902004.00 Subsurface water was not encountered during drilling. The borehole was backfilled with soil cuttings after drilling activities Driller: T. Timmermann Date Drilled: 10/10/2024 were completed. Logged by: J. Barnes Boring Depth: 10 feet Equipment: B-57 Boring Elevation: Ground Surface Hammer Type: Automatic Coordinates: Longitude: -98.1893 Latitude: 29.6053 Delayed Water Level: N/A Drilling Method: Solid Flight Auger w/SPT Sampling Encount. Cave-In at Time of Drilling: Delayed Water Observation Date: N/A SAMPLE DATA BORE/CORE DATA ELEVATION (ft) DEPTH (ft) GRAPHIC LOG ATTERBERG LIMITS (%) DRY DENSITY (pcf) SHEAR STRENGTH (psf) FAILURE STRAIN (%) MOISTURE CONTENT **MATERIALS DESCRIPTION** 1st 6" 2nd 6" 3rd 6" RQD LIQUID Report: AEP-GEOTECH LOG - LAT LONG % REC N-VALUE BLOWS/FT LL PL ы SANDY LEAN CLAY; stiff, dark brown (CL) 4-5-6 9 FAT CLAY; stiff to hard, dark brown to light brown and light gray (CH) 20/1/25 6-7-8 20 11 64 44 N = 15X:2024/09/24-09-02004.00 - LENNAR - ANN AUSTIN/GEOTECHNICAL/DATA\00240902004.00 -- HUNTER CREEK ANN AUSTIN.GPJ 6 - 10 - 14 95.2 19 N = 24 9 - 18 - 23 15 66 19 47 N = 41calcareous below 81/2 feet 10 - 13 - 19 15 N = 3210 Boring terminated at 10 feet. 11



Lennar **Ann Austin and Hunter Creek Subdivions** Weil Road

Log of B-15

Santa Clara, Gudalupe County, Texas

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Drilling	Co.:	TTL	., Inc.	TTL Project No.: 0	0240902004.00		Remarks: Subsurface water was no	ot encount	ered du	rina drillina	The
Driller:		T. 7	- Timmermann	Date Drilled: 1	0/10/2024		borehole was backfilled were completed.				
Logge	d by:	J. E	Barnes	Boring Depth: 1	0 feet						
Equipn	ment:	B-5	7	Boring Elevation: G	Ground Surface						
Hamm	ner Typ	e: <i>Aut</i>	omatic	Coordinates:	Longitude: -98.18	870 Lati	tude: 29.6018				
Drilling	Metho	od: Solid	d Flight Auger w/SPT Sampling			ot ncount.	▼ Delayed Water	Level:	N/A		
					Drilling: N/	Ά	Delayed Water Ob	servatio	n Dat	e: <i>N/A</i>	
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	ATIO ft)	DEPTH (ft)) Hd	POOT	MATERIALS DESCRIPTION	ш	BORE/	COR	E DATA	RI FI	AT LI	TERBE IMITS (RG %)	_	T.	분르	JRE	SING
9NG	ELEVATION (ft)	DEP	GR/	5	MATERIALO DESGRIF FISIT	TYPE	1st 6" 2nd 6" 3rd 6"	- TONS/SI	RQD % REC	OISTI CONTE (%)	LIQUID LIMIT	_	PLASTICITY INDEX	DRY DENSITY (pcf)	SHEAL RENG (psf)	STRA (%)	CONFINING PRESSURE (psi)	% PASSING #200 SIEVE
ATLC			///	////	LEAN CLAY; firm, dark brown (CL)	-	N-VALUE BLOWS/FT	<u>a.</u>	% REC	∑O	LL	PL	PI	<u> </u>	STS		88	%#
7-9C					,, (0_)													
CHLC		- 1	-///			V	2-	.3.3										
EOTE						ΙĂ	N	3 - 3 = 6		16								92.7
Report: AEP-GEOTECH LOG - LAT LONG		- 2			EAT CLAV stiff to hard dark brown to brown and gray	\vdash												
eport:/					FAT CLAY; stiff to hard, dark brown to brown and gray (CH)													
		- 3	-//			$ \rangle /$	4	4-5										
20/1/25						ΙĂ	N N	= 9		20	72	21	51					
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ANN AUSTINIGEOTECHNICALIDATA\00240902004.00 HUNTER CREEK ANN AUSTINI.GPJ																		
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HUNT		- 7			- becomes light brown and light gray below 6½ feet	\mathbb{N}												
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AL\D		– 9				X	8 - 1 N :	12 - 16 = 28	5	19								
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EOTE(— 10			Boring terminated at 10 feet.													
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Log of B-16

Santa Clara, Gudalupe County, Texas Page 1 of 1 Remarks: Drilling Co.: TTL, Inc. TTL Project No.: 00240902004.00 Subsurface water was not encountered during drilling. The borehole was backfilled with soil cuttings after drilling activities Driller: T. Timmermann Date Drilled: 10/10/2024 were completed. Logged by: J. Barnes Boring Depth: 10 feet Equipment: B-57 Boring Elevation: Ground Surface Hammer Type: Automatic Longitude: -98.1886 Latitude: 29.6028 Coordinates: Delayed Water Level: N/A Drilling Method: Solid Flight Auger w/SPT Sampling Encount. Cave-In at Time of Drilling: Delayed Water Observation Date: N/A SAMPLE DATA BORE/CORE DATA ELEVATION (ft) DEPTH (ft) GRAPHIC LOG ATTERBERG LIMITS (%) DRY DENSITY (pcf) SHEAR STRENGTH (psf) FAILURE STRAIN (%) MOISTURE CONTENT **MATERIALS DESCRIPTION** 1st 6" 2nd 6" 3rd 6" RQD LIQUID Report: AEP-GEOTECH LOG - LAT LONG % REC N-VALUE BLOWS/FT LL PL ы LEAN CLAY WITH SAND; stiff to hard, brownish-gray (CL) 2-4-8 84.0 6 2 3 20/1/25 8-8-8 7 17 27 44 4 X:2024/09/24-09-02004.00 - LENNAR - ANN AUSTIN/GEOTECHNICAL/DATA\00240902004.00 -- HUNTER CREEK ANN AUSTIN.GPJ 5 15 - 27 - 30 5 N = 57 6 38 - 50/4 N = 50/4" 7 6 8 FAT CLAY; very stiff, light brown (CH) 9 - 13 - 13 10 56 18 38 93.3 N = 2610 Boring terminated at 10 feet. 11 12 13 14



Log of B-17

Santa Clara, Gudalupe County, Texas Page 1 of 1 Remarks: Drilling Co.: TTL, Inc. TTL Project No.: 00240902004.00 Subsurface water was not encountered during drilling. The borehole was backfilled with soil cuttings after drilling activities Driller: T. Timmermann Date Drilled: 10/10/2024 were completed. Logged by: J. Barnes Boring Depth: 10 feet Equipment: B-57 Boring Elevation: Ground Surface Hammer Type: Automatic Coordinates: Longitude: -98.1895 Latitude: 29.6043 Delayed Water Level: N/A Drilling Method: Solid Flight Auger w/SPT Sampling Encount. Cave-In at Time of Drilling: Delayed Water Observation Date: N/A SAMPLE DATA BORE/CORE DATA ELEVATION (ft) DEPTH (ft) GRAPHIC LOG ATTERBERG LIMITS (%) DRY DENSITY (pcf) SHEAR STRENGTH (psf) FAILURE STRAIN (%) MOISTURE CONTENT **MATERIALS DESCRIPTION** 1st 6" 2nd 6" 3rd 6" RQD LIQUID Report: AEP-GEOTECH LOG - LAT LONG % REC N-VALUE BLOWS/FT LL PL ы CLAYEY SAND; medium dense, brownish-gray (SC) 3-6-13 6 N = 19 2 LEAN CLAY; hard, brownish-gray to light brown (CL) 3 20/1/25 13 - 20 - 17 8 N = 374 X:2024\09\24-09-02004.00 - LENNAR - ANN AUSTIN\GEOTECHNICAL\DATA\00240902004.00 -- HUNTER CREEK ANN AUSTIN\GPJ 22 - 50/5 5 N = 50/5'6 96.2 6 7 9 - 25 - 27 9 49 16 33 N = 528 FAT CLAY; hard, light brown (CH) 11 - 18 - 22 10 16 35 51 N = 4010 Boring terminated at 10 feet. 11 12 13 14



Log of **B-18**

Santa Clara, Gudalupe County, Texas

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Remarks: Drilling Co.: TTL, Inc. TTL Project No.: 00240902004.00 Subsurface water was not encountered during drilling. The borehole was backfilled with soil cuttings after drilling activities Driller: T. Timmermann Date Drilled: 10/11/2024 were completed. Logged by: A. DeLeon Boring Depth: 10 feet Equipment: B-57 Boring Elevation: Ground Surface Hammer Type: Automatic Coordinates: Longitude: -98.1911 Latitude: 29.6051 Delayed Water Level: N/A Drilling Method: Solid Flight Auger w/SPT Sampling Encount. Cave-In at Time of Drilling: Delayed Water Observation Date: N/A SAMPLE DATA BORE/CORE DATA ELEVATION (ft) DEPTH (ft) GRAPHIC LOG ATTERBERG LIMITS (%) DRY DENSITY (pcf) SHEAR STRENGTH (psf) FAILURE STRAIN (%) MOISTURE CONTENT **MATERIALS DESCRIPTION** 1st 6" 2nd 6" 3rd 6" RQD LIQUID PLASTIC LIMIT Report: AEP-GEOTECH LOG - LAT LONG % REC N-VALUE BLOWS/FT LL PL ы SANDY FAT CLAY; soft, dark brown (CH) 2-2-2 12 65 21 44 FAT CLAY; stiff to very stiff, dark brown (CH) 20/1/25 3-4-7 14 96.7 N = 11X:2024/09/24-09-02004.00 - LENNAR - ANN AUSTIN/GEOTECHNICAL/DATA\00240902004.00 -- HUNTER CREEK ANN AUSTIN.GPJ 5 - 8 - 10 15 6 - 9 - 12 68 20 48 N = 21becomes dark brown, brown, and light brown, calcareous below 81/2 feet 4 - 9 - 18 8 N = 2710 Boring terminated at 10 feet. 11 12 13 14



Log of B-19

Santa Clara, Gudalupe County, Texas

Page 1 of 1

						•
Drilling Co.:	TTL,	Inc.	TTL Project No.: 002	40902004.00	Remarks:	ot encountered during drilling. The
Driller:	T. Ti	mmermann	Date Drilled: 10/	10/2024		with soil cuttings after drilling activities
Logged by:	J. Ba	arnes	Boring Depth: 10 t	^F eet		
Equipment:	B-57	,	Boring Elevation: Gro	und Surface		
Hammer Type	: Auto	matic	Coordinates: Lor	ngitude: -98.1898 Latit	tude: 29.6031	
Drilling Method	: Solid	Flight Auger w/SPT Sampling	∇ Water Level at Time	of Drilling: Not Encount.	▼ Delayed Water	Level: N/A
				rilling: <i>N/A</i>	Delayed Water Ob	servation Date: N/A
Z G					SAMPLE DAT	ΓΑ
(ft)	APHIC -0G	MATERIALS	DESCRIPTION	BORE/CORE DAT	ATTERBERG LIMITS (%)	SILVE SURE SURE SURE SURE SING SING

	z		·		·	SAMPLE DATA BORE/CORE DATA ROD I STREAM BORE/CORE DATA ROD I STREAM ROD I STRAIN ROD I STRAIN											
	ATIO	9 	(11)	GRAPHIC LOG	MATERIALS DESCRIPTION	ш	BORE/CORE	DATA	JRE	AT LI	TERBE MITS (9	RG %)	<u></u>	TH	RE IN	IING JRE	ING EVE
SNG	ELEVATION (ft)		7	GR/ L	WATERIALO DESCRITTORY	TYPE	2nd 6" 3rd 6" TONS/SC	RQD	IOISTI SONTE (%)	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX	DRY DENSITY (pcf)	SHEAR STRENGTH (psf)	FAILÚRE STRAIN (%)	CONFIN PRESSI (psi)	% PASSING #200 SIEVE
AT LC					SILTY CLAY; very stiff, brownish-gray, trace sand (CL-ML)		N-VALUE G: %	U NEO	≥∪	LL	PL	PI	 	S		ÖĒ	8#
1-90					(CL-ML)	<u> </u>											
ECHL		-	1 -			V	5 - 9 - 11		3								86.8
GEOT							N = 20										00.0
Report: AEP-GEOTECH LOG - LAT LONG		- :	2 -		LEAN CLAY; hard, brownish-gray (CL)	<u> </u>											
Repor						7											
20/1/25		- ;	3 -			IV.	12 - 17 - 17 N = 34		6	43	17	26					
20/						$/\!\!/$	14 - 04										
ЭРЈ		<u> </u>	4 -		FAT CLAY; hard, light brown (CH)												
STIN.			_														
NN AL		[;	o —			IX.	14 - 26 - 24 N = 50		7	50	16	34					
EEK A		L,	a -			$/\!\!\!/$											
ANN AUSTIN/GEOTECHNICAL\DATA\00240902004.00 HUNTER CREEK ANN AUSTIN.GPJ		'	J														
HUNT		<u>.</u>	7 -			$\mathbb{N}/$											
- 00.1						IX.	19 - 17 - 20 N = 37		8								95.4
90200		- ;	3 -			\triangle											
00240																	
DATA\		- !	9 -			\mathbb{N}	14 - 20 - 25										
NICAL)						ľ	N = 45		11								
TECH		<u> </u>	0 —		Boring terminated at 10 feet.	<u>/ \</u>											
NGEO					g												
USTIN		- 1	1 -	-													
NAR-		- 1	2 -	-													
- LEN																	
004.00		- 1	3 -	1													
-09-02																	
X:\2024\09\24-09-02004.00 - LENNAR -		- 1	4 -	-													
(:\2024																	
^ L	This	s borir	a loa	shall not be se	eparated from the corresponding Instrument of Service; no third party may rely upon	this b	orina loa or the correspo	ondina In:	strument	of Servi	ce abser	nt a writte	n TTL Se	condary	Client Ac	reemen	t.



Log of B-20

							Santa Clara, G	audalur	pe (County, Te	exas							Pag	je 1 o	f 1	
	Drillin	g Co.:	TTL	., Inc.			TTL Project No.:	0024	109	02004.00			Rema		ater w	as not e	encount	ered di	ırina dri	llina Ti	ne
	Driller	:	Т. Т	īmmei	rmann		Date Drilled:	10/10	0/2	024			boreh		backfi	lled with					
	Logge	ed by:	J. B	arnes	;		Boring Depth:	10 fe	et												
	Equip	ment:	B-5	7			Boring Elevation:	Grou	ınd	Surface											
	Hamn	Hammer Type: Automatic					Coordinates:	Lon	gitu	ıde: -98.1	888	Latitu	de: 2	9.601	7						
	Drilling	g Metho	od: Solia	l Flight A	Auger w	/SPT Sampling		ime of	f Di		ot ncou		▼ D	elaye	d Wa	ter Le	evel:	N/A			
								of Dri	lling	g: <i>N</i>	/A		Delay	/ed W	/ater	Obse	rvatio	n Dat	e:	N/A	
	z	(:											5	SAMP	LE C	ATA					
LONG	ELEVATIO (ft)	GRAPHIC LOG				MATERIALS	DESCRIPTION		TYPE	BORE/ 3d 6, grade, which was a second state of the second state of	COR	RQD RQD % REC	MOISTURE CONTENT (%)	LIQUID LIMIT	TERBE MITS (' PLASTIC LIMIT' PL		DENSITY (pcf)	SHEAR STRENGTH (psf)	FAILURE STRAIN (%)	CONFINING PRESSURE (psi)	% PASSING #200 SIEVE

z	£	₀				10055	- D	S	AMF	PLE D						
ELEVATION (ft)	DEPTH (ft)	GRAPHIC LOG	MATERIALS DESCRIPTION	TYPE	BORE	COKE	RQD RQD REC	MOISTURE CONTENT (%)	LIQUID	TERBE MITS (S		DRY DENSITY (pcf)	SHEAR STRENGTH (psf)	FAILURE STRAIN (%)	CONFINING PRESSURE (psi)	% PASSING #200 SIEVE
		//////	SANDY LEAN CLAY; very stiff, brownish-gray (CL)		BLOWS/FT				LL	FL	FI		0)		0 11	0.4
-	- 1				5 - N	- 8 - 14 I = 22		7	45	18	27					
	- 2		LEAN CLAY; hard, light brownish-gray to light brown (CL)													
	- 3	-			14 - N	- 15 - 18 I = 33		6								96
	- 4															
_	 5 -				14 - N	- 17 - 18 I = 35		8								
	- 6		FAT CLAY; hard to very stiff, light brown (CH)		\ 											
-	- 7				12 - N	- 14 - 18 I = 32		9	57	17	40					
_	- 8															
_	- 9				6 - N	- 8 - 11 I = 19		13								99
	— 10 -		Boring terminated at 10 feet.		Y											
_	- 11	-														
	10															
	- 12															
-	- 13	-														
-	- 14															
			eparated from the corresponding Instrument of Service; no third party may rely upon													



14

Lennar **Ann Austin and Hunter Creek Subdivions** Weil Road

Log of B-21

Santa Clara, Gudalupe County, Texas

Page 1 of 1

Remarks: Drilling Co.: TTL, Inc. TTL Project No.: 00240902004.00 Subsurface water was not encountered during drilling. The borehole was backfilled with soil cuttings after drilling activities Driller: T. Timmermann Date Drilled: 10/11/2024 were completed. Logged by: A. DeLeon Boring Depth: 10 feet Equipment: B-57 Boring Elevation: Ground Surface Hammer Type: Automatic Coordinates: Longitude: -98.1893 Latitude: 29.6007 Delayed Water Level: N/A Drilling Method: Solid Flight Auger w/SPT Sampling Encount. Cave-In at Time of Drilling: Delayed Water Observation Date: N/A SAMPLE DATA BORE/CORE DATA ELEVATION (ft) DEPTH (ft) GRAPHIC LOG ATTERBERG LIMITS (%) DRY DENSITY (pcf) SHEAR STRENGTH (psf) FAILURE STRAIN (%) MOISTURE CONTENT **MATERIALS DESCRIPTION** 1st 6" 2nd 6" 3rd 6" RQD LIQUID Report: AEP-GEOTECH LOG - LAT LONG % REC N-VALUE BLOWS/FT LL PL ы LEAN CLAY; very stiff to hard, brownish-gray (CL) 4 - 6 - 10 7 96.2 N = 16 2 - becomes light brownish-gray between $2 \ensuremath{\%}\xspace_2$ and 4 feet 3 20/1/25 9 - 11 - 12 8 16 44 28 N = 234 X:2024/09/24-09-02004.00 - LENNAR - ANN AUSTIN/GEOTECHNICAL/DATA\00240902004.00 -- HUNTER CREEK ANN AUSTIN.GPJ - becomes brownish-gray, calcareous between 41/2 and 6 feet 5 9 - 17 - 19 8 N = 36 6 7 10 - 23 - 21 8 95.0 N = 448 FAT CLAY; very stiff, light brown to light gray (CH) 9 - 13 - 14 20 81 22 59 N = 2710 Boring terminated at 10 feet. 11 12 13



20/1/25 Report: AEP-GEOTECH LOG - LAT LONG

X:2024/09/24-09-02004.00 - LENNAR - ANN AUSTIN/GEOTECHNICAL/DATA/00240902004.00 -- HUNTER CREEK ANN AUSTIN.GPJ

Lennar Ann Austin and Hunter Creek Subdivions Weil Road

Log of B-22

Santa Clara, Gudalupe County, Texas

Page 1 of 1

Remarks: Drilling Co.: TTL, Inc. TTL Project No.: 00240902004.00 Subsurface water was not encountered during drilling. The borehole was backfilled with soil cuttings after drilling activities Driller: T. Timmermann Date Drilled: 10/10/2024 were completed. Logged by: J. Barnes Boring Depth: 10 feet Equipment: B-57 Boring Elevation: **Ground Surface** Hammer Type: Automatic Coordinates: Longitude: -98.1901 Latitude: 29.6022 Delayed Water Level: N/A Drilling Method: Solid Flight Auger w/SPT Sampling Encount. ☑ Cave-In at Time of Drilling: Delayed Water Observation Date: N/A N/A CAMDI E DATA

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ATIO	₌	E.	H B	MATERIAL C DESCRIPTION		BORE/CORE DATA	쀭누	AT LI	TERBE	RG %)	>	Е	IJZ	S H	NG VE
ELEVATION		DEPTH (ft)	GRAPHIC LOG	MATERIALS DESCRIPTION	TYPE	BORE/CORE DATA	NSTU NNTE	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	DENSITY (pcf)	SHEAR STRENGTH (psf)	FE (%)	CONFINING PRESSURE (psi)	% PASSING #200 SIEVE
						N-VALUE i. % REC	_Q Ω	LL	PL	PI	<u> </u>	STR	7 S	O.R.	#20 #20
<u> </u>				LEAN CLAY WITH SAND; very stiff, brown (CL)											
50					7										
핇	ŀ	- 1 -			W	8 - 9 - 11 N = 20	4	40	19	21					
					$ \Lambda $	N = 20		10							
ZU1/ZS KeportAEP-GEOTECH LOG - LAT LONG ELE	-	- 2 -		LEAN CLAY; very stiff to hard, light brown (CL)											
por:/				LEAN CLAT, very suit to flatd, light blown (CL)											
2		- 3 -			$\mathbb{N}/$										
2/1/(2		3			X	8 - 10 - 12 N = 22	5								85.8
Ñ					$/ \setminus$										
3	ı	- 4 -													
AUS	-	- 5 -			V	18 - 26 - 26	6	43	16	27					
ANA					$ \Lambda $	N = 52	0	43	10	21					
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		- 7 -			X	23 - 19 - 24 N = 43	8								96.7
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100Z4															
A	-	- 9 -			$ \rangle $	17 20 24									
CAL					ľ	17 - 29 - 24 N = 53	11								
ANN AUSTINNGEO I ECHNICALUATANUZAUBUZUU4.UU – HUNTER CREEK ANN AUSTIN.GF2		- 10 -			\triangle										
		10		Boring terminated at 10 feet.											
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¥ Y	H	- 12 -													
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-60-4-03-		- 14 -													
4/09/2		14 -													
X:\Z024\09\Z4-09-02004.00 - LENNAK -															



Log of B-23

Santa Clara, Gudalupe County, Texas Page 1 of 1 Remarks: Drilling Co.: TTL, Inc. TTL Project No.: 00240902004.00 Subsurface water was not encountered during drilling. The borehole was backfilled with soil cuttings after drilling activities Driller: T. Timmermann Date Drilled: 10/11/2024 were completed. Logged by: A. DeLeon Boring Depth: 10 feet Equipment: B-57 Boring Elevation: Ground Surface Hammer Type: Automatic Coordinates: Longitude: -98.1915 Latitude: 29.6042 Delayed Water Level: N/A Drilling Method: Solid Flight Auger w/SPT Sampling Encount. Cave-In at Time of Drilling: Delayed Water Observation Date: N/A SAMPLE DATA BORE/CORE DATA ELEVATION (ft) DEPTH (ft) GRAPHIC LOG ATTERBERG LIMITS (%) DRY DENSITY (pcf) SHEAR STRENGTH (psf) FAILURE STRAIN (%) MOISTURE CONTENT **MATERIALS DESCRIPTION** 1st 6" 2nd 6" 3rd 6" RQD LIQUID PLASTIC LIMIT Report: AEP-GEOTECH LOG - LAT LONG % REC N-VALUE BLOWS/FT LL PL Ы FAT CLAY; stiff, brown, calcareous (CH) 4-5-6 13 54 18 36 2 LEAN CLAY; very stiff, brown to light brown, calcareous (CL) 3 20/1/25 8 - 9 - 14 7 97.4 N = 234 X:2024\09\24-09-02004.00 - LENNAR - ANN AUSTIN\GEOTECHNICAL\DATA\00240902004.00 -- HUNTER CREEK ANN AUSTIN\GPJ 5 7-8-9 10 6 LEAN CLAY WITH SAND; hard, gray (CL) 7 10 - 15 - 21 9 81.1 N = 368 FAT CLAY; hard, light brown and light gray (CH) 17 - 25 - 36 50 16 34 11 N = 6110 Boring terminated at 10 feet. 11 12 13 14



Log of B-24

						/eil R								D-	4 -	£ 4	
Drilling	a Co .	TTI	, Inc.		Santa Clara, C			-	Rem	arks:				Pa	ge 1 o	T 1	
Driller			-	rmann	TTL Project No.: Date Drilled:	10/1		02004.00	Subsu boreh	ırface v ole was	vater w s backfi	as not	encount th soil c	tered d uttings	uring dr after dr	illing. T illing ac	he tivitie
Logge			DeLeoi		Boring Depth:	10/ T		U2 4	were	comple	ted.						
Equip		B-5						Curfoso									
		pe: Auto		<u> </u>	Boring Elevation: Coordinates:			Surface ide: -98.1916 Latit	ude: 2	9 603	25						
		*		, Auger w/SPT Sampling	✓ Water Level at ⁻				▼ D			ater Lo	evel:	N/A			
Diming	y IVICII	ou. com	i iigiit i	riager war i damping	□ Cave-In at Time			Encount.	-	•			ervatio		to:	N/A	
_					- Cave-III at TIIIIe	, OI DIII	 	j. IVA	Dela	SAMI	PLE [пра	ile.	IVA	
ELEVATION (ft)	DEPTH (ft)	GRAPHIC LOG		MATERIALS	DESCRIPTION		TYPE	BORE/CORE DAT	MOISTURE CONTENT	LIQUID	TERBE IMITS (RG	, E	SHEAR STRENGTH	FAILURE STRAIN (%)	CONFINING PRESSURE (psi)	% PASSING
			FAT	CLAY WITH SAND; st	iff, brown (CH)			BLOWS/FT						0,			
	- 1						\bigvee	2 - 4 - 7 N = 11	12								
	- 2		LEA	N CLAY; stiff, brownish	-gray (CL)												
	- 3 -						M	7 - 6 - 7 N = 13	9	46	18	28					
	- 4 -						/ \ \										
	5 - - 6						$\backslash\!\!\!\backslash$	6 - 6 - 9 N = 15	9								9
	- 7		FAT	CLAY; stiff to hard, bro light brown (CH)	ownish-gray to brown an	nd	\bigvee	7-8-7	11	59	17	42					
	- 8						\mathbb{N}	N = 15	''	00	.,	72					
	- 9						\bigvee	14 - 19 - 22 N = 41	12								9
	 10			Boring termin	ated at 10 feet.		<u> </u>										
	- 11	1															
	- 12	-															
	- 13	-															
	- 14																
771.	harian ta				ant of Comicos no third party may	ralizzman	thia t	poring log or the corresponding	Instrumon	t of Son	ion abon	nt a weitt	on TT/ Si	l	Client A		Ļ



14

Lennar **Ann Austin and Hunter Creek Subdivions** Weil Road

Log of **B-25**

Santa Clara, Gudalupe County, Texas Page 1 of 1 Remarks: Drilling Co.: TTL, Inc. TTL Project No.: 00240902004.00 Subsurface water was not encountered during drilling. The borehole was backfilled with soil cuttings after drilling activities Driller: T. Timmermann Date Drilled: 10/11/2024 were completed. Logged by: A. DeLeon Boring Depth: 10 feet Equipment: B-57 Boring Elevation: Ground Surface Hammer Type: Automatic Coordinates: Longitude: -98.1931 Latitude: 29.6049 Delayed Water Level: N/A Drilling Method: Solid Flight Auger w/SPT Sampling Encount. Cave-In at Time of Drilling: Delayed Water Observation Date: N/A SAMPLE DATA BORE/CORE DATA ELEVATION (ft) DEPTH (ft) GRAPHIC LOG ATTERBERG LIMITS (%) DRY DENSITY (pcf) SHEAR STRENGTH (psf) FAILURE STRAIN (%) MOISTURE CONTENT **MATERIALS DESCRIPTION** 3rd 6" 1st 6" 2nd 6" RQD LIQUID Report: AEP-GEOTECH LOG - LAT LONG % REC N-VALUE BLOWS/FT LL PL Ы LEAN CLAY WITH SAND; very stiff to hard, dark brown (CL) 6-8-11 10 46 17 29 N = 19 2 3 20/1/25 14 - 17 - 19 6 N = 36FAT CLAY; very stiff, light brown and gray, calcareous X:2024/09/24-09-02004.00 - LENNAR - ANN AUSTIN/GEOTECHNICAL/DATA\00240902004.00 -- HUNTER CREEK ANN AUSTIN.GPJ (CH) 5 - 8 - 11 97.5 16 8 - 11 - 16 64 19 45 N = 276 - 9 - 13 18 N = 22 10 Boring terminated at 10 feet. 11 12 13



Log of **B-26**

Santa Clara, Gudalupe County, Texas

Page 1 of 1 Remarks: Drilling Co.: TTL, Inc. TTL Project No.: 00240902004.00 Subsurface water was not encountered during drilling. The borehole was backfilled with soil cuttings after drilling activities Driller: 10/11/2024 T. Timmermann Date Drilled: were completed. Logged by: A. DeLeon Boring Depth: 10 feet Equipment: B-57 Boring Elevation: Ground Surface Hammer Type: Automatic Longitude: -98.1907 Latitude: 29.5998 Coordinates: Delayed Water Level: N/A Drilling Method: Solid Flight Auger w/SPT Sampling Encount. Cave-In at Time of Drilling: Delayed Water Observation Date: N/A SAMPLE DATA BORE/CORE DATA ELEVATION (ft) DEPTH (ft) GRAPHIC LOG ATTERBERG LIMITS (%) DRY DENSITY (pcf) SHEAR STRENGTH (psf) FAILURE STRAIN (%) MOISTURE CONTENT **MATERIALS DESCRIPTION** 3rd 6" 1st 6" 2nd 6" RQD LIQUID PLASTIC LIMIT Report: AEP-GEOTECH LOG - LAT LONG % REC N-VALUE BLOWS/FT LL PL ы FAT CLAY; stiff to very stiff, dark brown to light brown 3-5-4 13 20/1/25 6-7-8 47 18 68 21 N = 15X:2024/09/24-09-02004.00 - LENNAR - ANN AUSTIN/GEOTECHNICAL/DATA\00240902004.00 -- HUNTER CREEK ANN AUSTIN.GPJ 5 - 8 - 12 92.9 21 N = 20 - calcareous below 61/2 feet 7 - 7 - 11 14 N = 187 - 11 - 15 16 73 19 54 N = 2610 Boring terminated at 10 feet. 11 12 13 14



Log of B-27

Santa Clara, Gudalupe County, Texas Page 1 of 1 Remarks: Drilling Co.: TTL, Inc. TTL Project No.: 00240902004.00 Subsurface water was not encountered during drilling. The borehole was backfilled with soil cuttings after drilling activities Driller: T. Timmermann Date Drilled: 10/11/2024 were completed. Logged by: A. DeLeon Boring Depth: 10 feet Equipment: B-57 Boring Elevation: Ground Surface Hammer Type: Automatic Longitude: -98.1919 Latitude: 29.6013 Coordinates: Delayed Water Level: N/A Drilling Method: Solid Flight Auger w/SPT Sampling Encount. Cave-In at Time of Drilling: Delayed Water Observation Date: N/A SAMPLE DATA BORE/CORE DATA ELEVATION (ft) DEPTH (ft) GRAPHIC LOG ATTERBERG LIMITS (%) DRY DENSITY (pcf) SHEAR STRENGTH (psf) FAILURE STRAIN (%) MOISTURE CONTENT **MATERIALS DESCRIPTION** 1st 6" 2nd 6" 3rd 6" RQD LIQUID Report: AEP-GEOTECH LOG - LAT LONG % REC N-VALUE BLOWS/FT LL PL ы FAT CLAY; very stiff to stiff, dark brown, trace gravel 3 - 9 - 10 11 N = 19 20/1/25 8 - 9 - 10 16 88.0 N = 19X:2024/09/24-09-02004.00 - LENNAR - ANN AUSTIN/GEOTECHNICAL/DATA\00240902004.00 -- HUNTER CREEK ANN AUSTIN.GPJ 3-4-6 17 12 55 38 LEAN CLAY WITH SAND; very stiff, brown and pale brown, calcareous (CL) 7 - 10 - 8 7 40 15 25 80.3 N = 18FAT CLAY WITH SAND; hard, light brown (CH) 13 - 15 - 18 13 N = 3310 Boring terminated at 10 feet. 11 12 13 14



Log of B-28

Santa Clara, Gudalupe County, Texas Page 1 of 1 Remarks: Drilling Co.: TTL, Inc. TTL Project No.: 00240902004.00 Subsurface water was not encountered during drilling. The borehole was backfilled with soil cuttings after drilling activities Driller: T. Timmermann Date Drilled: 10/11/2024 were completed. Logged by: A. DeLeon Boring Depth: 10 feet Equipment: B-57 Boring Elevation: Ground Surface Hammer Type: Automatic Coordinates: Longitude: -98.1933 Latitude: 29.6035 Delayed Water Level: N/A Drilling Method: Solid Flight Auger w/SPT Sampling Encount. Cave-In at Time of Drilling: Delayed Water Observation Date: N/A SAMPLE DATA BORE/CORE DATA ELEVATION (ft) DEPTH (ft) GRAPHIC LOG ATTERBERG LIMITS (%) DRY DENSITY (pcf) SHEAR STRENGTH (psf) FAILURE STRAIN (%) MOISTURE CONTENT **MATERIALS DESCRIPTION** 1st 6" 2nd 6" 3rd 6" RQD LIQUID Report: AEP-GEOTECH LOG - LAT LONG % REC N-VALUE BLOWS/FT LL PL ы FAT CLAY; stiff to very stiff, dark brown, slightly calcareous (CH) 4-5-6 13 20/1/25 8 - 10 - 12 18 37 13 55 N = 22LEAN CLAY; hard, light brown, calcareous (CL) X:2024\09\24-09-02004.00 - LENNAR - ANN AUSTIN\GEOTECHNICAL\DATA\00240902004.00 -- HUNTER CREEK ANN AUSTIN\GPJ 5 9 - 18 - 30 97.6 8 N = 48 6 14 - 22 - 32 8 N = 548 FAT CLAY; hard, light brown (CH) 9 - 14 - 21 14 17 40 57 N = 3510 Boring terminated at 10 feet. 11 12 13 14



20/1/25 Report: AEP-GEOTECH LOG - LAT LONG

X:\2024\09\24-09-02004.00 - LENNAR - ANN AUSTIN\GEOTECHNICAL\DATA\00240902004.00 -- HUNTER CREEK ANN AUSTIN\GPJ

Lennar Ann Austin and Hunter Creek Subdivions Weil Road

Santa Clara, Gudalupe County, Texas

Road

Log of B-29

Page 1 of 1

Remarks: Drilling Co.: TTL, Inc. TTL Project No.: 00240902004.00 Subsurface water was not encountered during drilling. The borehole was backfilled with soil cuttings after drilling activities Driller: T. Timmermann Date Drilled: 10/11/2024 were completed. Logged by: A. DeLeon Boring Depth: 10 feet Equipment: B-57 Boring Elevation: **Ground Surface** Hammer Type: Automatic Coordinates: Longitude: -98.1924 Latitude: 29.5988 Delayed Water Level: N/A Drilling Method: Solid Flight Auger w/SPT Sampling Encount. ☑ Cave-In at Time of Drilling: Delayed Water Observation Date: N/A N/A

				= cave in at rime of B	T	9. 7471			: AME	PLE D						
NOL	(L)	일				BORE/CC	RE DATA	\\	AT				_	l	ு ய்	ΩШ
ELEVATION (ft)	DEPTH (ft)	GRAPHIC LOG	MATERIALS	DESCRIPTION	TYPE	BORE/CC	RQD	STUR NTEN (%)	LIQUID	PLASTIC LIMIT	PLASTICITY	NSITY pcf)	SHEAR STRENGTH (psf)	ILÚRE 'RAIN (%)	CONFINING PRESSURE (psi)	% PASSING #200 SIEVE
	Δ				F	N-VALUE di BLOWS/FT di	% REC	MO	LLL	PL	PI		STRE	FA	CON PRE	% P/ #200
5			SILTY CLAYEY SAND; me (SC-SM)	dium dense, brownish-gray												
			(======,													
	- 1 -				$ \rangle$	8 - 6 - N = 1	. 5 1	4								46.8
					$ \rangle$											
ELE ENGLISHER GEORGE EN LONG	- 2 -		SILTY CLAY WITH SAND; (CL-ML)	very stiff, brownish-gray		<u> </u>										
0			(CL-IVIL)													
	- 3 -				$ \rangle$	5-9- N=2	11	6	25	20	5					
Ď,					$ \rangle $	N = 2	U									
	- 4 -		LEAN CLAY; stiff to very sti	iff, brownsih-gray (CL)	-	<u>V</u>										
	— 5 —				V	5 - 7 - N = 1	8	10								86.8
						N = 1	5									00.0
	- 6 -					<u>\</u>										
						7										
	- 7 -				V	8 - 10 -	10	_	40	40	00					
						N = 2	0	7	48	16	32					
	- 8 -				<u> </u>	\										
74			- becomes light brown and	grav, calcareous below 81/		7										
	- 9 -		feet	gray, calcal cods below 0/2	$ \cdot $	0 12	14									
					ΙŇ	8 - 13 - N = 2	7	16								
	— 10 —		Davin a taunain	entend at 10 fact	<u> </u>	V										
			Boring termin	ated at 10 feet.												
	- 11 -															
2	- 12 -															
	12															
	- 13 -															
00.400000	13															
	14															
2001	- 14 -															
V: KOZ																



Log of B-30

Santa Clara, Gudalupe County, Texas

Page 1 of 1 Remarks: Drilling Co.: TTL, Inc. TTL Project No.: 00240902004.00 Subsurface water was not encountered during drilling. The borehole was backfilled with soil cuttings after drilling activities Driller: T. Timmermann Date Drilled: 10/11/2024 were completed. Logged by: A. DeLeon Boring Depth: 10 feet Equipment: B-57 Boring Elevation: Ground Surface Latitude: 29.5999 Hammer Type: Automatic Coordinates: Longitude: -98.1920 ▼ Delayed Water Level: N/A Drilling Method: Solid Flight Auger w/SPT Sampling Encount. Cave-In at Time of Drilling: Delayed Water Observation Date: N/A SAMPLE DATA BORE/CORE DATA ELEVATION (ft) DEPTH (ft) GRAPHIC LOG ATTERBERG LIMITS (%) MOISTURE CONTENT **MATERIALS DESCRIPTION** 1st 6" 2nd 6" 3rd 6" RQD LIQUID PLASTIC LIMIT Report: AEP-GEOTECH LOG - LAT LONG % REC N-VALUE BLOWS/FT LL PL ы FAT CLAY; stiff to very stiff, dark brown (CH) 4-4-5 12 20/1/25 6-6-7 16 97.3 X:2024/09/24-09-02004.00 - LENNAR - ANN AUSTIN/GEOTECHNICAL/DATA\00240902004.00 -- HUNTER CREEK ANN AUSTIN.GPJ 6-7-9 69 18 51 15 4 - 9 - 15 15 98.3 N = 24- becomes light brown and light gray below 81/2 feet 10 - 13 - 15 69 19 50 17 N = 28 10 Boring terminated at 10 feet. 11 12 13 14



Log of B-31

Santa Clara, Gudalupe County, Texas Page 1 of 1 Remarks: Drilling Co.: TTL, Inc. TTL Project No.: 00240902004.00 Subsurface water was not encountered during drilling. The borehole was backfilled with soil cuttings after drilling activities Driller: T. Timmermann Date Drilled: 10/12/2024 were completed. Logged by: A. DeLeon Boring Depth: 10 feet Equipment: B-57 Boring Elevation: Ground Surface Hammer Type: Automatic Longitude: -98.1937 Latitude: 29.5992 Coordinates: ▼ Delayed Water Level: N/A Drilling Method: Solid Flight Auger w/SPT Sampling Encount. Cave-In at Time of Drilling: Delayed Water Observation Date: N/A SAMPLE DATA BORE/CORE DATA ELEVATION (ft) DEPTH (ft) GRAPHIC LOG ATTERBERG LIMITS (%) DRY DENSITY (pcf) SHEAR STRENGTH (psf) FAILURE STRAIN (%) MOISTURE CONTENT **MATERIALS DESCRIPTION** 1st 6" 2nd 6" 3rd 6" RQD LIQUID PLASTIC LIMIT Report: AEP-GEOTECH LOG - LAT LONG % REC N-VALUE BLOWS/FT LL PL ы FAT CLAY; stiff to very stiff, dark brown (CH) 4-4-7 16 20/1/25 7 - 9 - 10 15 N = 19LEAN CLAY; very stiff, pale brown to dark brown, X:2024\09\24-09-02004.00 - LENNAR - ANN AUSTIN\GEOTECHNICAL\DATA\00240902004.00 -- HUNTER CREEK ANN AUSTIN\GPJ calcareous, trace gravel (CL) 5 8-7-9 16 90.4 45 29 13 6 7 - 12 - 16 12 N = 288 FAT CLAY; hard, light brown, trace sand (CH) 9 - 15 - 18 9 56 17 39 91.1 N = 3310 Boring terminated at 10 feet. 11 12 13 14



Lennar **Ann Austin and Hunter Creek Subdivions** Weil Road

Log of B-32

Santa Clara, Gudalupe County, Texas

Page 1 of 1

Drilling Co.:	TTL, Inc	2 .	TTL Project No.:	0024	0902004.	00	Remarks: Subsurface water was not encountered during drilling. The			
Driller:	T. Timm	nermann	Date Drilled:	10/12	2/2024		borehole was backfilled with soil cuttings after drilling activities were completed.			
Logged by:	A. DeLe	eon	Boring Depth:	10 fe	et					
Equipment:	B-57		Boring Elevation:	Grou	ınd Surfac	e				
Hammer Type	: Automa	tic	Coordinates:	Long	gitude: -98	3.1935 Latit	ude: 29.6005			
Drilling Method	: Solid Fligh	ht Auger w/SPT Sampling	abla Water Level at Ti	ime of	f Drilling:	Not Encount.	▼ Delayed Water Level: N/A			
	Delayed Water Observation Date: N/A									
SAMPLE DATA										

	z						S	AMF		ATA					
LONG	ELEVATION (ft)	DEPTH (ft)	GRAPHIC LOG	MATERIALS DESCRIPTION	TYPE	BORE/CORE DATA *50 to 50 September 100 Sept	MOISTURE CONTENT (%)	AT LI LIQUID LIMIT	TERBE MITS (9 PLASTIC LIMIT	RG %) PLASTICITY INDEX PI	DRY DENSITY (pcf)	SHEAR STRENGTH (psf)	FAILURE STRAIN (%)	CONFINING PRESSURE (psi)	% PASSING #200 SIEVE
-LAT				LEAN CLAY; stiff to hard, dark brown to light brown, trace sand (CL)		BOWSHI									
Report: AEP-GEOTECH LOG - LAT LONG		- 1 -		1400 oand (OL)	\bigvee	5 - 8 - 6 N = 14	10								90.4
t:AEP-GEO		- 2 -			\triangle										
20/1/25 Repor		- 3 -			\bigvee	8-6-7	6	37	17	20					
		- 4 -			\triangle	N = 13	ŭ	01		20					
AUSTIN.GP		— 5 —			\bigvee	9 - 17 - 23	_								
REEK ANN		- 6 -			\triangle	N = 40	7								94.6
HUNTER C		- 7 -			\ \/										
02004.00		- 8 -			\bigwedge	11 - 25 - 29 N = 54	9	41	15	26					
4TA\002409		- 9 -			\ /										
ANN AUSTINIGEOTECHNICAL\DATA\00240902004.00 - HUNTER CREEK ANN AUSTINIGPJ					\mathbb{N}	18 - 25 - 25 N = 50	9								
rin/GEOTE		— 10 —		Boring terminated at 10 feet.											
- ANN AUS		- 11 -													
- LENNAR		- 12 -	-												
09-02004.00		- 13 -	-												
X:\2024\09\24-09-02004.00 - LENNAR		- 14 -													
×L	This	horing log	chall not be e	eparated from the corresponding Instrument of Service: no third party may rely upon	thic h	oring log or the corresponding In	etrumont	of Sonii	co abcor	nt a umitto	n TTI So	condany	Cliont Ac	vroomont	



Log of B-33

Santa Clara, Gudalupe County, Texas Page 1 of 1 Remarks: Drilling Co.: TTL, Inc. TTL Project No.: 00240902004.00 Subsurface water was not encountered during drilling. The borehole was backfilled with soil cuttings after drilling activities Driller: T. Timmermann Date Drilled: 10/12/2024 were completed. Logged by: A. DeLeon Boring Depth: 10 feet Equipment: B-57 Boring Elevation: Ground Surface Hammer Type: Automatic Coordinates: Longitude: -98.1934 Latitude: 29.6019 Delayed Water Level: N/A Drilling Method: Solid Flight Auger w/SPT Sampling Encount. Cave-In at Time of Drilling: Delayed Water Observation Date: N/A SAMPLE DATA BORE/CORE DATA ELEVATION (ft) DEPTH (ft) GRAPHIC LOG ATTERBERG LIMITS (%) DRY DENSITY (pcf) SHEAR STRENGTH (psf) FAILURE STRAIN (%) MOISTURE CONTENT **MATERIALS DESCRIPTION** 1st 6" 2nd 6" 3rd 6" RQD LIQUID Report: AEP-GEOTECH LOG - LAT LONG % REC N-VALUE BLOWS/FT LL PL Ы FAT CLAY; stiff to very stiff, brown (CH) 4-6-6 10 55 18 37 20/1/25 8 - 8 - 11 94.0 12 N = 19LEAN CLAY; stiff to very stiff, pale brown to brown, X:2024\09\24-09-02004.00 - LENNAR - ANN AUSTIN\GEOTECHNICAL\DATA\00240902004.00 -- HUNTER CREEK ANN AUSTIN\GPJ calcareous (CL) 5 6-7-7 9 46 15 31 6 - becomes hard between 61/2 and 8 feet 10 - 10 - 21 8 98.0 N = 318 - becomes light brown below 81/2 and 10 feet (CL) 9 10 - 14 - 15 11 N = 29 10 Boring terminated at 10 feet. 11 12 13 14



Log of B-34

Santa Clara, Gudalupe County, Texas Page 1 of 1 Remarks: Drilling Co.: TTL, Inc. TTL Project No.: 00240902004.00 Subsurface water was not encountered during drilling. The borehole was backfilled with soil cuttings after drilling activities Driller: T. Timmermann Date Drilled: 10/12/2024 were completed. Logged by: A. DeLeon Boring Depth: 10 feet Equipment: B-57 Boring Elevation: Ground Surface Hammer Type: Automatic Coordinates: Longitude: -98.1950 Latitude: 29.6010 ▼ Delayed Water Level: N/A Drilling Method: Solid Flight Auger w/SPT Sampling Encount. Cave-In at Time of Drilling: Delayed Water Observation Date: N/A SAMPLE DATA BORE/CORE DATA ELEVATION (ft) DEPTH (ft) GRAPHIC LOG ATTERBERG LIMITS (%) DRY DENSITY (pcf) SHEAR STRENGTH (psf) FAILURE STRAIN (%) MOISTURE CONTENT **MATERIALS DESCRIPTION** 1st 6" 2nd 6" 3rd 6" RQD LIQUID PLASTIC LIMIT Report: AEP-GEOTECH LOG - LAT LONG % REC N-VALUE BLOWS/FT LL PL ы FAT CLAY; stiff, dark brown (CH) 3-4-6 10 2 LEAN CLAY; stiff to hard, gray, calcareous (CL) 3 20/1/25 6-5-5 6 87.3 N = 104 X:2024\09\24-09-02004.00 - LENNAR - ANN AUSTIN\GEOTECHNICAL\DATA\00240902004.00 -- HUNTER CREEK ANN AUSTIN\GPJ 5 12 - 14 - 17 8 15 29 44 N = 31 6 7 14 - 17 - 19 11 95.3 N = 368 FAT CLAY WITH SAND; hard, brownish-gray (CH) 15 - 19 - 20 53 16 37 11 N = 3910 Boring terminated at 10 feet. 11 12 13 14



Log of B-35

Santa Clara, Gudalupe County, Texas Page 1 of 1 Remarks: Drilling Co.: TTL, Inc. TTL Project No.: 00240902004.00 Subsurface water was not encountered during drilling. The borehole was backfilled with soil cuttings after drilling activities Driller: T. Timmermann Date Drilled: 10/12/2024 were completed. Logged by: A. DeLeon Boring Depth: 10 feet Equipment: B-57 Boring Elevation: Ground Surface Hammer Type: Automatic Coordinates: Longitude: -98.1948 Latitude: 29.6024 Delayed Water Level: N/A Drilling Method: Solid Flight Auger w/SPT Sampling Encount. Cave-In at Time of Drilling: Delayed Water Observation Date: N/A SAMPLE DATA BORE/CORE DATA ELEVATION (ft) DEPTH (ft) GRAPHIC LOG ATTERBERG LIMITS (%) DRY DENSITY (pcf) SHEAR STRENGTH (psf) FAILURE STRAIN (%) (%) CONFINING PRESSURE MOISTURE CONTENT **MATERIALS DESCRIPTION** 1st 6" 2nd 6" 3rd 6" RQD LIQUID Report: AEP-GEOTECH LOG - LAT LONG % REC N-VALUE BLOWS/FT LL PL ы LEAN CLAY; stiff to very stiff, gray to light brown, trace sand (CL) 4-6-6 7 93.9 2 3 20/1/25 6 - 11 - 15 4 40 17 23 N = 264



Log of B-36

Santa Clara, Gudalupe County, Texas Page 1 of 1 Remarks: Drilling Co.: TTL, Inc. TTL Project No.: 00240902004.00 Subsurface water was not encountered during drilling. The borehole was backfilled with soil cuttings after drilling activities Driller: T. Timmermann Date Drilled: 10/12/2024 were completed. Logged by: A. DeLeon Boring Depth: 10 feet Equipment: B-57 Boring Elevation: Ground Surface Hammer Type: Automatic Coordinates: Longitude: -98.1967 Latitude: 29.6023 Delayed Water Level: N/A Drilling Method: Solid Flight Auger w/SPT Sampling Encount. Cave-In at Time of Drilling: Delayed Water Observation Date: N/A SAMPLE DATA BORE/CORE DATA ELEVATION (ft) DEPTH (ft) GRAPHIC LOG ATTERBERG LIMITS (%) DRY DENSITY (pcf) SHEAR STRENGTH (psf) FAILURE STRAIN (%) MOISTURE CONTENT **MATERIALS DESCRIPTION** 1st 6" 2nd 6" 3rd 6" RQD LIQUID Report: AEP-GEOTECH LOG - LAT LONG % REC N-VALUE BLOWS/FT LL PL ы FAT CLAY WITH SAND; stiff, dark brown (CH) 5-6-7 14 61 20 41 2 LEAN CLAY; very stiff to hard, pale brown and gray to light brown (CL) 3 20/1/25 7 - 10 - 14 5 95.9 N = 244 X:2024/09/24-09-02004.00 - LENNAR - ANN AUSTIN/GEOTECHNICAL/DATA\00240902004.00 -- HUNTER CREEK ANN AUSTIN.GPJ 5 7 - 13 - 15 8 N = 28 6 19 - 26 - 33 42 15 27 N = 59 8 9 16 - 22 - 25 9 96.1 N = 47 10 Boring terminated at 10 feet. 11 12 13 14



Log of B-37

Santa Clara, Gudalupe County, Texas

Page 1 of 1

Remarks: Drilling Co.: TTL, Inc. TTL Project No.: 00240902004.00 Subsurface water was not encountered during drilling. The borehole was backfilled with soil cuttings after drilling activities Driller: T. Timmermann Date Drilled: 10/12/2024 were completed. Logged by: A. DeLeon Boring Depth: 10 feet Equipment: B-57 Boring Elevation: Ground Surface Hammer Type: Automatic Coordinates: Longitude: -98.1964 Latitude: 29.6034 Delayed Water Level: N/A Drilling Method: Solid Flight Auger w/SPT Sampling Encount. Cave-In at Time of Drilling: Delayed Water Observation Date: N/A SAMPLE DATA BORE/CORE DATA ELEVATION (ft) DEPTH (ft) GRAPHIC LOG ATTERBERG LIMITS (%) DRY DENSITY (pcf) SHEAR STRENGTH (psf) FAILURE STRAIN (%) MOISTURE CONTENT **MATERIALS DESCRIPTION** 1st 6" 2nd 6" 3rd 6" RQD LIQUID Report: AEP-GEOTECH LOG - LAT LONG % REC N-VALUE BLOWS/FT LL PL ы FAT CLAY; stiff to hard, dark brown to brown (CH) 4-5-6 18 20/1/25 6 - 8 - 10 20 19 68 48 N = 18X:2024/09/24-09-02004.00 - LENNAR - ANN AUSTIN/GEOTECHNICAL/DATA\00240902004.00 -- HUNTER CREEK ANN AUSTIN.GPJ 7 - 12 - 20 95.8 17 - calcareous between 61/2 and 8 feet 6 - 16 - 20 14 N = 36- becomes light brown and light gray below 81/2 feet 11 - 16 - 17 60 17 43 17 N = 3310 Boring terminated at 10 feet. 11 12 13 14



Log of B-38

Santa Clara, Gudalupe County, Texas

Page 1 of 1

Remarks: Drilling Co.: TTL, Inc. TTL Project No.: 00240902004.00 Subsurface water was not encountered during drilling. The borehole was backfilled with soil cuttings after drilling activities Driller: T. Timmermann Date Drilled: 10/12/2024 were completed. Logged by: A. DeLeon Boring Depth: 10 feet Equipment: B-57 Boring Elevation: Ground Surface Hammer Type: Automatic Coordinates: Longitude: -98.1949 Latitude: 29.6041 Delayed Water Level: N/A Drilling Method: Solid Flight Auger w/SPT Sampling Encount. Cave-In at Time of Drilling: Delayed Water Observation Date: N/A SAMPLE DATA BORE/CORE DATA ELEVATION (ft) DEPTH (ft) GRAPHIC LOG ATTERBERG LIMITS (%) MOISTURE CONTENT DRY DENSITY (pcf) SHEAR STRENGTI (psf) FAILURE STRAIN (%) **MATERIALS DESCRIPTION** 1st 6" 2nd 6" 3rd 6" RQD LIQUID Report: AEP-GEOTECH LOG - LAT LONG % REC N-VALUE BLOWS/FT LL PL ы FAT CLAY; stiff to very stiff, dark brown to brown (CH) 4-6-8 95.7 14 - trace gravel between 21/2 and 4 feet 20/1/25 5 - 10 - 12 9 N = 22X:2024/09/24-09-02004.00 - LENNAR - ANN AUSTIN/GEOTECHNICAL/DATA\00240902004.00 -- HUNTER CREEK ANN AUSTIN.GPJ 6 - 9 - 11 42 60 18 14 N = 20 - becomes hard between 61/2 and 8 feet 9 - 17 - 21 13 67 18 49 N = 38- becomes light brown and light gray below 81/2 feet 7 - 11 - 16 28 89.3 N = 2710 Boring terminated at 10 feet. 11 12 13 14



Log of B-40

					Santa Clara, C	Gudalupe	Coun	ty, Texas						Pag	e 1 of	1				
Drilling Co.: TTL, Inc.			TTL Project No.: 00240902004.00 Remarks: Subsurface water was not encountered during											ring drilling. The						
Driller: T. Timmermann			Date Drilled:	lled with	d with soil cuttings after drilling activities															
Logged by: A. DeLeon			Boring Depth:	10 fee	t															
Equip	ment:	B-57	•		Boring Elevation:	Groun	d Sur	face												
Hamn	ner Typ	oe: Autoi	matic		Coordinates:	Longi	tude:	-98.1975 Lat	itude: 2	9.604	1 1									
Drilling Method: Solid Flight Auger w/SPT Sampling						Time of [Drilling	g: Not	▼ D	elaye	ed Wa	ter Le	er Level: <i>N/A</i>							
					of Drillir	ng:	Encount. N/A	Dela	Delayed Water Observation Date: N/A											
Z	t)	0							SAMPLE DATA											
ELEVATION (ft)	DEРТН (ft)	GRAPHIC LOG		MATERIALS	DESCRIPTION	Z N	N-VA N-VB N-VB N-VB		— [হু হু হ		TERBE IMITS (* PLASTIC LIMIT		DRY DENSITY (pcf)	SHEAR STRENGTH (psf)	FAILURE STRAIN (%)	CONFINING PRESSURE (psi)	% PASSING			
	1		FAT (CLAY; stiff to hard, dar	k brown (CH)		1	<u> </u>												
	- 2 -							5 - 5 - 5 N = 10	12								94			
	- 3 -							7 - 7 - 11 N = 18	11	58	18	40								
	- 4 -					/		N IC												
	— 5 —							9 - 13 - 20 N = 33	15								97			
	- 6 -					/	7													
	- <i>/</i> - - 8 -							9 - 20 - 23 N = 43	12											
	- 9 -		- beco	omes light brown and l	light gray below 8⅓ feet	t		9 - 21 - 23 N = 44	17	60	18	42								
	— 10 —			Doring town:	atod at 10 fact	/														
				boning termina	ated at 10 feet.															
	- 11 -																			
	- 12 -	-																		
	- 13 -																			
	– 14 -	_																		
This	horing log	shall not be sen	narated fr	om the corresponding Instrume	ent of Service; no third party may	roly upon this	horing	log or the correspondi	na Instrumen	t of Son	rice ahser	at a writte	n TTI Se	condan	Client A	aroomon	L			



Log of B-41

Santa Clara, Gudalupe County, Texas

Page 1 of 1

Remarks: Drilling Co.: TTL, Inc. TTL Project No.: 00240902004.00 Subsurface water was not encountered during drilling. The borehole was backfilled with soil cuttings after drilling activities Driller: T. Timmermann Date Drilled: 10/12/2024 were completed. Logged by: A. DeLeon Boring Depth: 10 feet Equipment: B-57 Boring Elevation: Ground Surface Hammer Type: Automatic Coordinates: Longitude: -98.1963 Latitude: 29.6050 Delayed Water Level: N/A Drilling Method: Solid Flight Auger w/SPT Sampling Encount. Cave-In at Time of Drilling: Delayed Water Observation Date: N/A SAMPLE DATA ELEVATION (ft) DEPTH (ft) GRAPHIC LOG ATTERBERG LIMITS (%) BORE/CORE DATA DRY DENSITY (pcf) SHEAR STRENGTH (psf) FAILURE STRAIN (%) MOISTURE CONTENT **MATERIALS DESCRIPTION** 1st 6" 2nd 6" 3rd 6" RQD LIQUID PLASTIC LIMIT Report: AEP-GEOTECH LOG - LAT LONG % REC N-VALUE BLOWS/FT LL PL ы CLAYEY SAND; loose, dark brown (SC) 2-4-6 10 FAT CLAY; stiff to very stiff, dark brown (CH) 20/1/25 5-5-7 95.2 18 N = 12X:2024/09/24-09-02004.00 - LENNAR - ANN AUSTIN/GEOTECHNICAL/DATA\00240902004.00 -- HUNTER CREEK ANN AUSTIN.GPJ 5 - 8 - 10 74 19 55 16 - becomes hard and highly calcareous between 61/2 and 8 feet 10 - 16 - 19 13 69 18 51 N = 35- becomes light brown and light gray below 81/2 feet 9 - 13 - 14 18 N = 2710 Boring terminated at 10 feet. 11 12 13 14



10

11

12

13

14

Lennar **Ann Austin and Hunter Creek Subdivions**

Log of B-42

98.2

Weil Road Santa Clara, Gudalupe County, Texas Page 1 of 1 Remarks: Drilling Co.: TTL, Inc. TTL Project No.: 00240902004.00 Subsurface water was not encountered during drilling. The borehole was backfilled with soil cuttings after drilling activities Driller: T. Timmermann Date Drilled: 10/13/2024 were completed. Logged by: A. DeLeon Boring Depth: 10 feet Equipment: B-57 Boring Elevation: Ground Surface Hammer Type: Automatic Coordinates: Longitude: -98.1973 Latitude: 29.6053 Delayed Water Level: N/A Drilling Method: Solid Flight Auger w/SPT Sampling Encount. Cave-In at Time of Drilling: Delayed Water Observation Date: N/A SAMPLE DATA BORE/CORE DATA ELEVATION (ft) DEPTH (ft) GRAPHIC LOG ATTERBERG LIMITS (%) DRY DENSITY (pcf) SHEAR STRENGTH (psf) FAILURE STRAIN (%) MOISTURE CONTENT **MATERIALS DESCRIPTION** 1st 6" 2nd 6" 3rd 6" RQD LIQUID Report: AEP-GEOTECH LOG - LAT LONG % REC N-VALUE BLOWS/FT LL PL ы LEAN CLAY; very stiff, dark brown to gray (CL) 6 - 10 - 11 9 N = 21 2 3 20/1/25 10 - 11 - 13 7 17 88.8 40 23 N = 24FAT CLAY; hard to very stiff, brown to brown and light X:2024/09/24-09-02004.00 - LENNAR - ANN AUSTIN/GEOTECHNICAL/DATA\00240902004.00 -- HUNTER CREEK ANN AUSTIN.GPJ gray, calcareous (CH)

Boring terminated at 10 feet.

19 50



Log of B-43

Santa Clara, Gudalupe County, Texas

Page 1 of 1

					Santa Clara, Gudai	upe County, Texas		Page 1 of 1						
Drilling Co.: TTL, Inc.					TTL Project No.: 002	240902004.00	Remarks: Subsurface water was not encountered during drilling. The							
Driller: T. Timmermann			immermann	Date Drilled: 10/	13/2024	borehole was backfilled with soil cuttings after drilling activities were completed.								
Logged by: A. DeLeon				DeLeon	Boring Depth: 10									
	Equip	ment:	B-5	7	Boring Elevation: Gro	ound Surface								
Hammer Type: Automatic					Coordinates: Lo	ngitude: -98.1969 Latit	rude: 29.6064							
	Drilling	g Metho	od: Solia	l Flight Auger w/SPT Sampling	$ oxedsymbol{ox{oxed}}}}} } \mathbf{oxedsymbol{oxedsymbol{ox{W}}}} $ Watter Level at Time	of Drilling: Not Encount.	▼ Delayed Water	Level: N/A						
						rilling: N/A	Delayed Water Ob	servation Date: N/A						
	ELEVATION (ft)	DЕРТН (ft)	GRAPHIC LOG	MATERIALS	DESCRIPTION	BORE/CORE DAT		SING SING						
LONG GRA GRA						HODE SO	LIQUID PLASTIC PLAST IND	STANDEN DEN STANDER ST						

z									SAME	PLE C						
ONG ELEVATION	€	DEPTH (ft)		GRAPHIC LOG	MATERIALS DESCRIPTION	TYPE	BORE/CORE DAT	TURE (S	AT L	TERBE IMITS (RG %)	SITY	AR AGTH	ÚRE (S)	INING SURE si)	% PASSING #200 SIEVE
LONG		В		р		ĭ		MOIS CON	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY	DRY DENSITY (pcf)	SHEAR STRENGTH (psf)	STR (%	CONFI PRESS (ps	% PAS #200 \$
- LAT					LEAN CLAY; very stiff to hard, dark brown to light brown (CL)											
SH LOG		- 1	_			\mathbb{N}										
EOTEC						$ \lambda $	8 - 10 - 14 N = 24	6								
Report:AEP-GEOTECH LOG - LAT LONG ELE		- 2	-													
Report					- becomes brownish-gray between 21/2 and 4 feet											
20/1/25		- 3					8 - 10 - 14 N = 24	6								91.3
70		- 4				$\backslash \backslash$										
Y.GPJ		7														
AUSTIN		— 5				\mathbb{N}	18 - 30 - 40									
X ANN							N = 70	6	38	15	23					
ANN AUSTINIGEOTECHNICALIDATA\00240902004.00 HUNTER CREEK ANN AUSTIN.GPJ		- 6	-													
UNTER		_														
H 00		- 7	_				30 - 31 - 35 N = 66	11								95.6
902004		- 8				V										
\00240					FAT CLAY; hard, light brown and light gray (CH)											
-\DATA		- 9	-			V	18 - 23 - 26	9	54	17	37					
HNICA							N = 49				01					
ЕОТЕС		— 10			Boring terminated at 10 feet.											
STING		- 11	_													
NN AU																
		- 12	! -													
- LENI																
2004.00	-	- 13	-													
24-09-0		- 14														
X:\2024\09\24-09-02004.00 - LENNAR -		14														
X:\20	This	horing	loa s	hall not he se	eparated from the corresponding Instrument of Service; no third party may rely upon	this !	poring log or the corresponding	Instrumen	t of Serv	ice abse	nt a writte	en TTL Se	econdary	Client Ac	reemen	,



20/1/25 Report: AEP-GEOTECH LOG - LAT LONG

X:2024/09/24-09-02004.00 - LENNAR - ANN AUSTIN/GEOTECHNICAL/DATA/00240902004.00 -- HUNTER CREEK ANN AUSTIN.GPJ

Lennar Ann Austin and Hunter Creek Subdivions Weil Road

Log of B-44

Santa Clara, Gudalupe County, Texas

Page 1 of 1

Remarks: Drilling Co.: TTL, Inc. TTL Project No.: 00240902004.00 Subsurface water was not encountered during drilling. The borehole was backfilled with soil cuttings after drilling activities Driller: T. Timmermann Date Drilled: 10/13/2024 were completed. Logged by: A. DeLeon Boring Depth: 10 feet Equipment: B-57 Boring Elevation: **Ground Surface** Hammer Type: Automatic Coordinates: Longitude: -98.1985 Latitude: 29.6057 Delayed Water Level: N/A Drilling Method: Solid Flight Auger w/SPT Sampling Encount. ☑ Cave-In at Time of Drilling: Delayed Water Observation Date: N/A N/A CAMDI E DATA

z						S	AMF		ATA					
D F (:	#) #	일일	MATERIAL O DECORIDADA		BORE/CORE DATA	\ \ 	AT L	TERBE MITS (9	RG %)	\	Ε	ш¬	S H	ВÄ
ELEVATION (ft)	DEPTH (ft)	GRAPHIC LOG	MATERIALS DESCRIPTION	TYPE	1st 6" 2nd 6" 3rd 6" ONS/SQF	STU NTE (%)	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX	JRY NSIT (pcf)	EAR ENG' psf)	ilur Trair (%)	IFINI SSU psi)	ASSI SIE
				-	BORE/CORE DATA	ΘΩ O	LIMIT	PL	PI	DRY DENSITY (pcf)	SHEAR STRENGTH (psf)	FA	CONFINING PRESSURE (psi)	% PASSING #200 SIEVE
ZU/1/23 Keport/AEP-GEO/1ECH LUG - LA I LONG			LEAN CLAY; stiff to hard, gray to brown and gray (CL)		BEONGITT									
<u>.</u>														
길	- 1			\mathbb{N}										
				I X	5 - 6 - 10 N = 16	8	45	18	27					
2 2				$ / \rangle$										
취	- 2	-/////		\vdash										
DOC.														
				N/										
1/25	- 3			I V	9 - 13 - 16 N = 29	6								96.5
Ž				$ /\rangle$	IN - 29									
_	- 4	-/////		igspace										
				$\mathbb{N}/$										
P	- 5 -			ΙV	14 - 16 - 22	10								
Z Z				$ \Lambda $	N = 38									
7	- 6			igspace										
בֿן צו														
				∇										
티	- 7	- //////		W	20 - 24 - 26	9	49	17	32					
00.4				$ \Lambda $	N = 50		40	.,	02					
020	- 8			\square										
72408														
AUC			- becomes light brown and light gray below 8½ feet	∇										
P P	- 9	*/////		IV	19 - 29 - 34 N = 63	10								96.4
				$ \Lambda $	N = 63	10								30.4
ANN AUS INVGEO IECHNICALUAI AVUZAUBUZUU4.UU – HUNI EK CKEEK ANN AUS IIN.GFZ	_ 10 -			\bigsqcup										
			Boring terminated at 10 feet.											
2														
	- 11	-												
Z														
	- 12													
N N N N N N N N N N N N N N N N N N N		1												
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74-0. X	- 14													
409		1												
K:\Z0Z4\U9\Z4-U9-UZUU4.U0 - LENNAK -														



Log of B-45

Santa Clara, Gudalupe County, Texas

Page 1 of 1

Remarks: Drilling Co.: TTL, Inc. TTL Project No.: 00240902004.00 Subsurface water was not encountered during drilling. The borehole was backfilled with soil cuttings after drilling activities Driller: T. Timmermann Date Drilled: 10/11/2024 were completed. Logged by: A. DeLeon Boring Depth: 10 feet Equipment: B-57 Boring Elevation: **Ground Surface** Hammer Type: Automatic Coordinates: Longitude: -98.1984 Latitude: 29.6069 Delayed Water Level: N/A Drilling Method: Solid Flight Auger w/SPT Sampling Encount. ☑ Cave-In at Time of Drilling: Delayed Water Observation Date: N/A N/A

	Z	(;						SAM	PLE [ATA					
ONG	ELEVATION (ft)	DEPTH (ft)	GRAPHIC LOG	MATERIALS DESCRIPTION	TYPE	BORE/CORE D/	MOISTURE	% LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	DRY DENSITY (pcf)	SHEAR STRENGTH (psf)	FAILURE STRAIN (%)	CONFINING PRESSURE (psi)	% PASSING #200 SIEVE
LATL				SILTY CLAY; very stiff, dark brown (CL-ML)		BLOWS/FT			rL	1 1		0)			0. #-
Report: AEP-GEOTECH LOG - LAT LONG		- 1 -				5-7-9 N=16	7								92.7
rt:AEP		- 2 -		LEAN CLAY WITH SAND; very stiff to hard, brownish-gray (CL)	\vdash										
Repo				brownisn-gray (CL)											
20/1/25		- 3 - - 4 -				9 - 10 - 12 N = 22	5	36	16	20					
GPJ		4													
ANN AUSTINIGEOTECHNICALIDATA\00240902004.00 HUNTER CREEK ANN AUSTINI.GPJ		E													
NN AL		— 5 —			IX.	9 - 17 - 17 N = 34	7								
EK A					//										
3 CRE		- 6 -		FAT CLAY; hard to very stiff, brownish-gray (CH)											
JNTE															
0 H		- 7 -			ΙV	13 - 16 - 17 N = 33	1								92.9
004.0					$ /\rangle$	14 – 30									
40902		- 8 -			r	<u>\</u>									
A\002															
L\DAT		- 9 -			IV	9 - 14 - 15	1	2 55	17	38					
INICA						N = 29									
TECF		— 10 —		Boring terminated at 10 feet.	+										
NGEC															
USTI		- 11 -	-												
A NN															
		- 12 -	-												
LENN															
4.00 -		- 13 -	-												
3-0200															
1/24-0		- 14 -	-												
X:\2024\09\24-09-02004.00 - LENNAR -															
Σ̄! Χ	This	horing log	shall not be s	eparated from the corresponding Instrument of Service; no third party may rely upon	this	haring log or the correspond	lina Instrun	ent of Sen	vice abse	nt a writte	an TTI Se	condany	Client A	aroomon	<u> </u>



Log of B-46

Santa Clara, Gudalupe County, Texas Page 1 of 1 Remarks: Drilling Co.: TTL, Inc. TTL Project No.: 00240902004.00 Subsurface water was not encountered during drilling. The borehole was backfilled with soil cuttings after drilling activities Driller: T. Timmermann Date Drilled: 10/11/2024 were completed. Logged by: A. DeLeon Boring Depth: 10 feet Equipment: B-57 Boring Elevation: Ground Surface Hammer Type: Automatic Coordinates: Longitude: -98.1995 Latitude: 29.6073 Delayed Water Level: N/A Drilling Method: Solid Flight Auger w/SPT Sampling Encount. Cave-In at Time of Drilling: Delayed Water Observation Date: N/A SAMPLE DATA BORE/CORE DATA ELEVATION (ft) DEPTH (ft) GRAPHIC LOG ATTERBERG LIMITS (%) DRY DENSITY (pcf) SHEAR STRENGTH (psf) FAILURE STRAIN (%) MOISTURE CONTENT **MATERIALS DESCRIPTION** 1st 6" 2nd 6" 3rd 6" RQD LIQUID PLASTIC LIMIT Report: AEP-GEOTECH LOG - LAT LONG % REC N-VALUE BLOWS/FT LL PL ы SILTY CLAY; very stiff, gray to pale brown, calcareous (CL-ML) 6 - 9 - 13 5 N = 22 2 - becomes pale brown between 21/2 and 4 feet 3 20/1/25 8 - 13 - 16 4 95.2 N = 294 SANDY LEAN CLAY; hard, light brown (CL) X:2024/09/24-09-02004.00 - LENNAR - ANN AUSTIN/GEOTECHNICAL/DATA\00240902004.00 -- HUNTER CREEK ANN AUSTIN.GPJ 5 19 - 36 - 50/5 17 5 33 16 N = 86/11" 6 50/5 N = 50/5"4 8 LEAN CLAY; hard, light brown (CL) 29 - 50/4 9 N = 50/4" 8 39 15 24 91.6 10 Boring terminated at 10 feet. 11 12 13 14



20/1/25 Report: AEP-GEOTECH LOG - LAT LONG

X:2024/09/24-09-02004.00 - LENNAR - ANN AUSTIN/GEOTECHNICAL/DATA/00240902004.00 -- HUNTER CREEK ANN AUSTIN.GPJ

Lennar Ann Austin and Hunter Creek Subdivions Weil Road

Log of B-47

Santa Clara, Gudalupe County, Texas

Page 1 of 1

Remarks: Drilling Co.: TTL, Inc. TTL Project No.: 00240902004.00 Subsurface water was not encountered during drilling. The borehole was backfilled with soil cuttings after drilling activities Driller: T. Timmermann Date Drilled: 10/11/2024 were completed. Logged by: A. DeLeon Boring Depth: 10 feet Equipment: B-57 Boring Elevation: Ground Surface Hammer Type: Automatic Coordinates: Longitude: -98.1983 Latitude: 29.6083 Delayed Water Level: N/A Drilling Method: Solid Flight Auger w/SPT Sampling Encount. ☑ Cave-In at Time of Drilling: Delayed Water Observation Date: N/A N/A CAMDI E DATA

	z				SAMPLE DATA BORE/CORE DATA										
	ATIO	€	l H _S S	MATERIALS DESCRIPTION		BORE/CORE DATA	뽒늗	AT LI	TERBE MITS (9	RG 6)	≥	~ ∓	KE N	NG RE	NG
٥	ELEVATION (ft)	DEPTH (ft)	GRAPHIC LOG	WATERIALS DESCRIPTION	TYPE	1st 6" 2nd 6" 3rd 6" ONS/SQI	SNTE (%)	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	DRY DENSITY (pcf)	SHEAR STRENGTH (psf)	AILUF TRAI (%)	CONFINING PRESSURE (psi)	% PASSING #200 SIEVE
Ź	ш					N-VALUE 6. % REC	88	LL	PL	PI	ä	STR	S	OR.	#20 #20
ZU/1/25 REPOITAEP-GEUTECH LUG - LAT LUNG				LEAN CLAY; stiff to very stiff, dark brown to brownish-gray, calcareous (CL)											
3				(∇										
5	•	- 1			IV.	3 - 4 - 6 N = 10	9								
						N = 10									
Ä		- 2			igwdap										
) DOLL															
2		- 3			$\mathbb{N}/$										
27/1/2		3			I X	7 - 8 - 6 N = 14	7	38	15	23					
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2		- 4			Н										
5 2					\vdash										
ACS	-	- 5 -	-{//////		V	8 - 10 - 13									00.7
ANA					$ \Lambda $	N = 23	9								98.7
A I		- 6			$/ \setminus$										
ANN AUS IINGEO I ECHNICALIDA I AGUZZGUGA. 00 HUNI EK CKEEK ANN AUS IINGGPJ				FAT CLAY; hard to very stiff, brownish-gray to light brown and light gray (CH)											
		_			N/										
		- 7			I V	10 - 13 - 18 N = 31	10	54	17	37					
0.40					$ /\rangle$	14-31									
0802		- 8	-/////		\vdash										
10024															
<u> </u>		- 9	-/////		\mathbb{N}	40.0.40									
ZAL Z					ΙX	10 - 9 - 13 N = 22	21								97.9
		— 10 -			$/ \setminus$										
		_ 10 -		Boring terminated at 10 feet.											
5															
200	•	- 11	-												
•	•	- 12	_												
- 00:		- 13													
72004															
4-09-1															
109/2		- 14	1												
X:\Z0Z4\U9\Z4-09-0Z004.00 - LENNAK															
اخ															

	T									Sheet	
Boring	Depth	USCS	Water Content (%)	Liquid Limit	Plastic Limit	Plasticity Index	% Gravel	% Sand	Maximum Size (mm)	% Passing #200 % Silt % Clay (If hydrometer data available)	D: (m
B-01	0.5 - 2		18						0.075	94.7	-
B-01	4.5 - 6		16	54	18	36					-
B-01	6.5 - 8		10						0.075	68.2	-
B-01	8.5 - 10		12	66	19	47					-
B-02	2.5 - 4		8	68	19	49					-
B-02	4.5 - 6		18						0.075	81.8	-
B-02	6.5 - 8		20	70	23	47					-
B-03	2.5 - 4		15	64	18	46					-
B-03	4.5 - 6		13						0.075	97.2	-
B-03	8.5 - 10		16	69	19	50					-
B-04	0.5 - 2		11	26	22	4					-
B-04	2.5 - 4		14						0.075	96.6	-
B-04	4.5 - 6		14	66	19	47					-
B-04	6.5 - 8		18						0.075	92.9	-
B-05	0.5 - 2		17						0.075	97.6	-
B-05	2.5 - 4		23	72	21	51					-
B-05	4.5 - 6		21						0.075	96.2	-
B-05	6.5 - 8		14	69	23	46					-
B-06	2.5 - 4		22						0.075	91.1	-
B-06	4.5 - 6		23	74	24	50					_
B-06	6.5 - 8		25						0.075	93.3	-
B-06	8.5 - 10		30	87	28	59					_
B-07	0.5 - 2		13						0.075	99.6	-
B-07	2.5 - 4		16	50	20	30					-
B-07	4.5 - 6		15						0.075	93.8	-
B-07	6.5 - 8		14	63	19	44					-
B-08	4.5 - 6	CL	7	44	16	28			0.075	57.1	-
B-08	8.5 - 10	СН	9	53	16	37			0.075	88.7	Γ.
B-09	0.5 - 2		10						0.075	91.7	_
B-09	2.5 - 4		12	70	22	48					-
B-09	6.5 - 8		7						0.075	89.4	-
B-09	8.5 - 10		8	52	17	35					-
B-10	0.5 - 2		13	67	21	46					-
B-10	4.5 - 6		29						0.075	88.0	-
B-10	6.5 - 8		23	71	21	50					-
B-11	0.5 - 2		15						0.075	92.8	
B-11	4.5 - 6		14	69	19	50					-
B-11	6.5 - 8		16						0.075	81.7	-
B-11	8.5 - 10		13	44	15	29					-
B-12	2.5 - 4		12						0.075	89.1	-
B-12	4.5 - 6		11	62	19	43					-
B-12	6.5 - 8		12	58	20	38					-



Client: Lennar

Project: Ann Austin and Hunter Creek Subdivions Location: Santa Clara, Gudalupe County, Texas

	T				T			Τ	Т	Sheet	7 01
Boring	Depth	USCS	Water Content (%)	Liquid Limit	Plastic Limit	Plasticity Index	% Gravel	% Sand	Maximum Size (mm)	% Passing #200 % Silt % Clay (If hydrometer data available)	Dt (m
B-13	4.5 - 6		18						0.075	96.7	-
B-13	6.5 - 8		16	76	24	52					-
B-13	8.5 - 10		19	67	18	49					-
B-14	2.5 - 4		11	64	20	44					-
B-14	4.5 - 6		19						0.075	95.2	-
B-14	6.5 - 8		15	66	19	47					-
B-15	0.5 - 2		16						0.075	92.7	-
B-15	2.5 - 4		20	72	21	51					-
B-15	4.5 - 6		14						0.075	94.0	-
B-15	6.5 - 8		13	62	18	44					-
B-16	0.5 - 2		6						0.075	84.0	-
B-16	2.5 - 4		7	44	17	27					-
B-16	8.5 - 10	CH	10	56	18	38			0.075	93.3	-
B-17	4.5 - 6		6						0.075	96.2	-
B-17	6.5 - 8		9	49	16	33					-
B-17	8.5 - 10		10	51	16	35					-
B-18	0.2 -			65	21	44					-
B-18	2.5 - 4		14						0.075	96.7	-
B-18	6.5 - 8		19	68	20	48					-
B-19	0.5 - 2		3						0.075	86.8	-
B-19	2.5 - 4		6	43	17	26					-
B-19	4.5 - 6		7	50	16	34					-
B-19	6.5 - 8		8						0.075	95.4	-
B-20	0.5 - 2		7	45	18	27					-
B-20	2.5 - 4		6						0.075	96.9	-
B-20	6.5 - 8		9	57	17	40					١.
B-20	8.5 - 10		13						0.075	99.1	
B-21	0.5 - 2		7						0.075	96.2	—
B-21	2.5 - 4		8	44	16	28					
B-21	6.5 - 8		8						0.075	95.0	-
B-21	8.5 - 10		20	81	22	59					-
B-22	0.5 - 2		4	40	19	21					
B-22	2.5 - 4		5						0.075	85.8	
B-22	4.5 - 6		6	43	16	27					١.
B-22	6.5 - 8		8						0.075	96.7	١.
B-23	0.5 - 2		13	54	18	36					١.
B-23	2.5 - 4		7						0.075	97.4	
B-23	6.5 - 8		9						0.075	81.1	١.
B-23	8.5 - 10		11	50	16	34					١.
B-24	2.5 - 4		9	46	18	28					١.
B-24	4.5 - 6		9						0.075	98.2	١.
B-24	6.5 - 8		11	59	17	42					١.



Client: Lennar

Project: Ann Austin and Hunter Creek Subdivions Location: Santa Clara, Gudalupe County, Texas

Borng Depth USCS Content (%) Umit Plesticity Plesticity Grove Sand (mm) Macodinum Plesticity Content (%) Umit Plesticity Grove Sand (mm) Macodinum Plesticity Content (mm) Plesticity Content (mm) Plesticity Plesticity										Sheet	3 of 4
B-25 0.5-2 10 46 17 29	Boring	Depth	USCS	Content			, , ,		Size	_	
B-25 4.5-6 16 0.075 97.5 B-26 6.5-8 12 64 19 45 </td <td>B-24</td> <td>8.5 - 10</td> <td></td> <td>12</td> <td></td> <td></td> <td></td> <td> </td> <td>0.075</td> <td>97.2</td> <td></td>	B-24	8.5 - 10		12				 	0.075	97.2	
B-25 6.5 - 8 12 64 19 45 <td>B-25</td> <td>0.5 - 2</td> <td></td> <td>10</td> <td>46</td> <td>17</td> <td>29</td> <td> </td> <td></td> <td></td> <td></td>	B-25	0.5 - 2		10	46	17	29	 			
B-26 2.5 - 4	B-25	4.5 - 6		16				 	0.075	97.5	
B-28 4.5 · 6 21 0.075 92.9 B-26 8.5 · 10 16 73 19 54	B-25	6.5 - 8		12	64	19	45	 			
B-26 8.5-10 16 73 19 54 -	B-26	2.5 - 4		18	68	21	47	 			
B-27 2.5-4 16 0.075 88.0 B-27 4.5-6 12 55 17 38 </td <td>B-26</td> <td>4.5 - 6</td> <td></td> <td>21</td> <td></td> <td></td> <td></td> <td> </td> <td>0.075</td> <td>92.9</td> <td></td>	B-26	4.5 - 6		21				 	0.075	92.9	
B-27 4.5 - 6 12 55 17 38 <td>B-26</td> <td>8.5 - 10</td> <td></td> <td>16</td> <td>73</td> <td>19</td> <td>54</td> <td> </td> <td></td> <td></td> <td></td>	B-26	8.5 - 10		16	73	19	54	 			
B-27 6.5 - 8 CL 7 40 15 25 0.075 80.3 B-28 2.5 - 4 13 55 18 37 <td>B-27</td> <td>2.5 - 4</td> <td></td> <td>16</td> <td></td> <td></td> <td></td> <td> </td> <td>0.075</td> <td>88.0</td> <td></td>	B-27	2.5 - 4		16				 	0.075	88.0	
B-28 2.5 - 4 13 55 18 37	B-27	4.5 - 6		12	55	17	38	 			
B-28 4.5 - 6 8 0.075 97.6 B-28 8.5 - 10 14 57 17 40	B-27	6.5 - 8	CL	7	40	15	25	 	0.075	80.3	
B-28 8.5-10 14 57 17 40 -	B-28	2.5 - 4		13	55	18	37	 			
B-29 2.5 - 4 6 25 20 5		4.5 - 6		8				 	0.075	97.6	
B-29 2.5 - 4 6 25 20 5	Б-28	8.5 - 10		14	57	17	40	 			
B-29 2.5 - 4 6 25 20 5	В-29 О	0.5 - 2		4				 	0.075	46.8	
B-30 6.5 - 8 15 0.075 98.3 B-30 8.5 - 10 17 69 19 50 0.075 90.4 B-31 4.5 - 6 CL 13 45 16 29 0.075 90.4 B-31 8.5 - 10 CH 9 56 17 39 0.075 91.1 B-32 0.5 - 2 10 0.075 90.4 B-32 2.5 - 4 6 37 17 20 0.075 94.6 B-32 6.5 - 8 9 41 15 26 0.075 94.6	' P 20	2.5 - 4			25	20	5	 			
B-30 6.5 - 8 15 0.075 98.3 B-30 8.5 - 10 17 69 19 50 0.075 90.4 B-31 4.5 - 6 CL 13 45 16 29 0.075 90.4 B-31 8.5 - 10 CH 9 56 17 39 0.075 91.1 B-32 0.5 - 2 10 0.075 90.4 B-32 2.5 - 4 6 37 17 20 0.075 94.6 B-32 6.5 - 8 9 41 15 26 0.075 94.6	B-29	4.5 - 6		10				 	0.075	86.8	
B-30 6.5 - 8 15 0.075 98.3 B-30 8.5 - 10 17 69 19 50 0.075 90.4 B-31 4.5 - 6 CL 13 45 16 29 0.075 90.4 B-31 8.5 - 10 CH 9 56 17 39 0.075 91.1 B-32 0.5 - 2 10 0.075 90.4 B-32 2.5 - 4 6 37 17 20 0.075 94.6 B-32 6.5 - 8 9 41 15 26 0.075 94.6	ഗ് B-29 ≓	6.5 - 8			48	16	32	 			
B-30 6.5 - 8 15 0.075 98.3 B-30 8.5 - 10 17 69 19 50 0.075 90.4 B-31 4.5 - 6 CL 13 45 16 29 0.075 90.4 B-31 8.5 - 10 CH 9 56 17 39 0.075 91.1 B-32 0.5 - 2 10 0.075 90.4 B-32 2.5 - 4 6 37 17 20 0.075 94.6 B-32 6.5 - 8 9 41 15 26 0.075 94.6	B-30	2.5 - 4						 	0.075	97.3	
B-30 8.5 - 10 17 69 19 50 B-31 4.5 - 6 CL 13 45 16 29 0.075 90.4 B-31 8.5 - 10 CH 9 56 17 39 0.075 91.1 B-32 0.5 - 2 10 0.075 90.4 B-32 2.5 - 4 6 37 17 20 0.075 94.6 B-32 6.5 - 8 9 41 15 26	B-30	4.5 - 6			69	18	51	 			
B-31	8-30 B-30	6.5 - 8						 	0.075	98.3	
B-31 8.5 - 10 CH 9 56 17 39 0.075 91.1 B-32 0.5 - 2 10 0.075 90.4 B-32 2.5 - 4 6 37 17 20 0.075 94.6 B-32 4.5 - 6 7 0.075 94.6 B-32 6.5 - 8 9 41 15 26	B-30	8.5 - 10						 			
B-31 8.5-10 CH 9 56 17 39 0.075 91.1 B-32 0.5-2 10 0.075 90.4 B-32 2.5-4 6 37 17 20 <td></td> <td>4.5 - 6</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td> </td> <td></td> <td></td> <td></td>		4.5 - 6						 			
B-32 0.5-2 10 0.075 90.4 B-32 2.5-4 6 37 17 20 <t< td=""><td><u>ජි</u> B-31</td><td>8.5 - 10</td><td>CH</td><td></td><td>56</td><td>17</td><td>39</td><td> </td><td></td><td></td><td></td></t<>	<u>ජි</u> B-31	8.5 - 10	CH		56	17	39	 			
8-32 2.5 - 4 6 37 17 20 -	B-32	0.5 - 2						 	0.075	90.4	
8-32 4.5-6 7 0.075 94.6 8-32 6.5-8 9 41 15 26 <td< td=""><td>ĕ B-32</td><td></td><td></td><td></td><td>37</td><td>17</td><td>20</td><td> </td><td></td><td></td><td></td></td<>	ĕ B-32				37	17	20	 			
B-32 6.5-8 9 41 15 26	▼ B-32 ₩	4.5 - 6						 	0.075	94.6	
8-33 0.5-2 10 55 18 37	B-32							 			
B-33 2.5 - 4 12 0.075 94.0 B-33 4.5 - 6 9 46 15 31	₩ B-33	0.5 - 2			55	18	37	 			
B-33 4.5-6 9 46 15 31	B-33 □							 			
B-33 6.5-8 8 0.075 98.0 B-34 2.5-4 6 0.075 87.3 B-34 4.5-6 8 44 15 29	B-33						31	 			
B-34 2.5 - 4 6 0.075 87.3 B-34 4.5 - 6 8 44 15 29 B-34 6.5 - 8 11 0.075 95.3 B-34 8.5 - 10 11 53 16 37 B-35 0.5 - 2 7 0.075 93.9 B-35 2.5 - 4 4 40 17 23 B-35 4.5 - 6 6	B-33	_									
B-34 4.5-6 8 44 15 29	50400 B-34										
B-34 6.5 - 8 11 0.075 95.3 B-34 8.5 - 10 11 53 16 37	Ŏ B-34										
B-34 8.5 - 10 11 53 16 37 <	B-34										
B-35 0.5 - 2 / 0.075 93.9 B-35 2.5 - 4 4 40 17 23 B-35 4.5 - 6 6 0.075 91.9 B-35 6.5 - 8 6 46 15 31 B-36 0.5 - 2 14 61 20 41 B-36 2.5 - 4 5 0.075 95.9 B-36 6.5 - 8 8 42 15 27	S B-34 로					_					
B-35	Ď B-35 ₩	_									
B-35	O B-35										
B-36 0.5 - 8 6 46 15 31	B-35										
B-36	D B-35										
B-36 6.5 - 8 8 42 15 27	B-36										
B-36 0.5 - 8 8 42 15 27	B-36	_									
	B-36	6.5 - 8		8 	42	15	27	 			



Client: Lennar

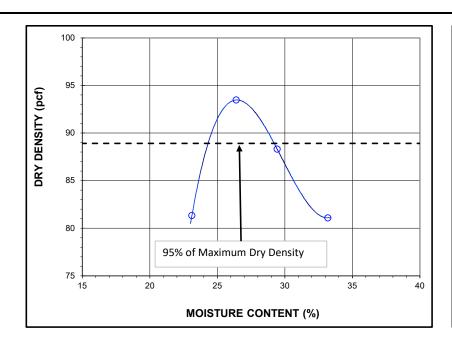
Project: Ann Austin and Hunter Creek Subdivions Location: Santa Clara, Gudalupe County, Texas

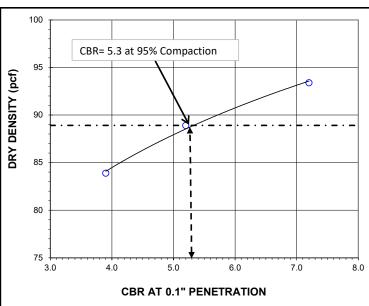
			I		ı			1		Sheet	4 of 4
Boring	Depth	USCS	Water Content (%)	Liquid Limit	Plastic Limit	Plasticity Index	% Gravel	% Sand	Maximum Size (mm)	% Passing #200 % Silt % Clay (If hydrometer data available)	D50 (mm)
B-36	8.5 - 10		9						0.075	96.1	
B-37	2.5 - 4		19	68	20	48					
B-37	4.5 - 6		17						0.075	95.8	
B-37	8.5 - 10		17	60	17	43					
B-38	0.5 - 2		14						0.075	95.7	
B-38	4.5 - 6		14	60	18	42					
B-38	6.5 - 8		13	67	18	49					
B-38	8.5 - 10		28						0.075	89.3	
B-40	0.5 - 2		12						0.075	94.6	
B-40	2.5 - 4		11	58	18	40					
B-40	4.5 - 6		15						0.075	97.6	
B-40	8.5 - 10		17	60	18	42					
B-41	2.5 - 4		18						0.075	95.2	
B-41	4.5 - 6		16	74	19	55					
B-41	6.5 - 8		13	69	18	51					
B-42	2.5 - 4	CL	7	40	17	23			0.075	88.8	
B-42	4.5 - 6		8						0.075	98.2	
B-42	6.5 - 8		9	69	19	50					
B-43	2.5 - 4		6						0.075	91.3	
B-43	4.5 - 6		6	38	15	23					
B-43	6.5 - 8		11						0.075	95.6	
B-43	8.5 - 10		9	54	17	37					
B-44	0.5 - 2		8	45	18	27					
B-44	2.5 - 4		6						0.075	96.5	
B-44	6.5 - 8		9	49	17	32					
B-44	8.5 - 10		10						0.075	96.4	
B-45	0.5 - 2		7						0.075	92.7	
B-45	2.5 - 4		5	36	16	20					
B-45	6.5 - 8		10						0.075	92.9	
B-45	8.5 - 10		12	55	17	38					
B-46	2.5 - 4		4						0.075	95.2	
B-46	4.5 - 6		5	33	17	16					
B-46	8.5 - 10	CL	8	39	15	24			0.075	91.6	
B-47	2.5 - 4		7	38	15	23					
B-47	4.5 - 6		9						0.075	98.7	
B-47	6.5 - 8		10	54	17	37					
B-47	8.5 - 10		21						0.075	97.9	
CBR-1	0 -	СН		59	30	29		4.0	4.75	96.0	
CBR-2	0 -	СН		57	26	31	1.4	5.6	38.1	93.0	
CBR-3	0 -	CH		64	31	33		2.3	4.75	97.7	
CBR-4	0 -	CL		45	24	21		21.1	4.75	78.9	



Client: Lennar

Project: Ann Austin and Hunter Creek Subdivions Location: Santa Clara, Gudalupe County, Texas





Proctor Test Method: Standard Proctor (ASTM D-698)
CBR Test Method: California Bearing Ration (ASTM D-1883)

Material: Dark Brown Fat Clay (CH)

CBR Sample Location: 29.6070°, -98.1856°

Sample Depth: Between 0 and 5 feet below existing ground surface Optimum Moisture Content: 26.7 % Maximum Dry Unit Weight: 93.6 pcf % Passing # 200 Sieve 96.0 %

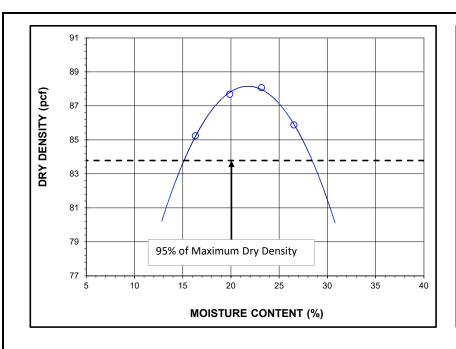
Atterberg Limits: LL = 60, PL = 30, PI = 29

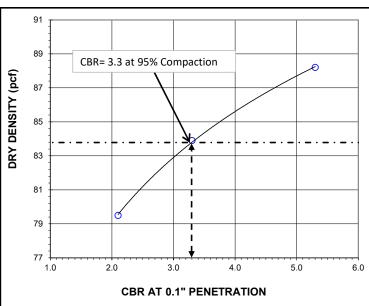


ANN AUSTIN AND HUNTER CREEK SUBDIVISIONS WEIL ROAD

SANTA CLARA, GUADALUPE COUNTY, TEXAS

Drawn By: RB
Checked By: TA
Proj No: 00240902004.00
File Name





Proctor Test Method: Standard Proctor (ASTM D-698) CBR Test Method: California Bearing Ration (ASTM D-1883)

Material: Brown Fat Clay (CH)

CBR Sample Location: 29.60417°, -98.1915°

Sample Depth: Between 0 and 5 feet below existing ground surface Optimum Moisture Content: 22.1 %

Maximum Dry Unit Weight: 88.2 pcf
% Passing # 200 Sieve 93.0 %

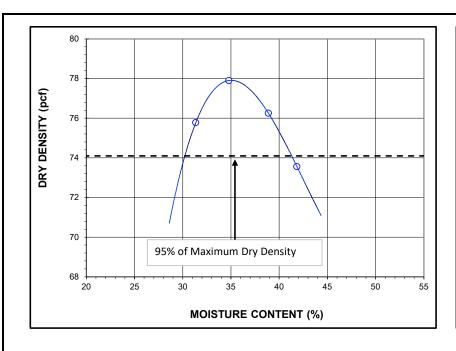
Atterberg Limits: LL = 57, PL = 26, PI = 31

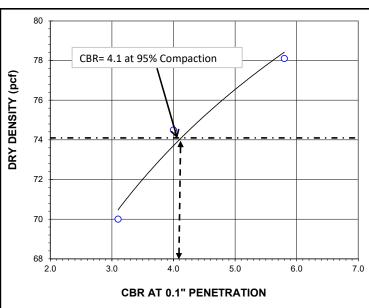


ANN AUSTIN AND HUNTER CREEK SUBDIVISIONS WEIL ROAD

SANTA CLARA, GUADALUPE COUNTY, TEXAS

Drawn By: RB
Checked By: TA
Proj No: 00240902004.00
File Name





Proctor Test Method: Standard Proctor (ASTM D-698) CBR Test Method: California Bearing Ration (ASTM D-1883)

Material: Dark Brown Fat Clay (CH)

CBR Sample Location: 29.5992°, -98.1937°

Sample Depth: Between 0 and 5 feet below existing ground surface Optimum Moisture Content: 35.2 % Maximum Dry Unit Weight: 78.0 pcf % Passing # 200 Sieve 97.7 %

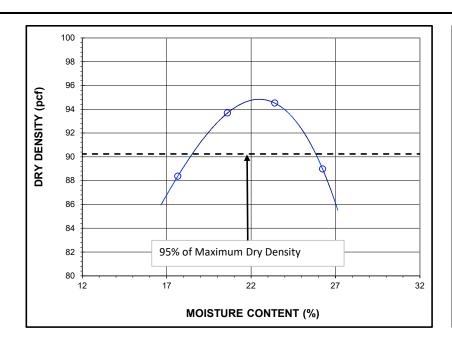
Atterberg Limits: LL = 64, PL = 31, PI = 33

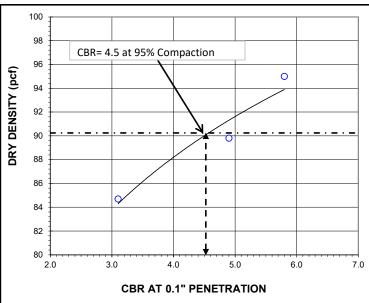


ANN AUSTIN AND HUNTER CREEK SUBDIVISIONS WEIL ROAD

SANTA CLARA, GUADALUPE COUNTY, TEXAS

Drawn By: RB
Checked By: TA
Proj No: 00240902004.00
File Name





Proctor Test Method: Standard Proctor (ASTM D-698) CBR Test Method: California Bearing Ration (ASTM D-1883)

Material: Light Brown Lean Clay with Sand (CL)

CBR Sample Location: 29.6057°, -98.1985°

Sample Depth: Between 0 and 5 feet below existing ground surface Optimum Moisture Content: 22.4 % Maximum Dry Unit Weight: 95.0 pcf % Passing # 200 Sieve 78.9 %

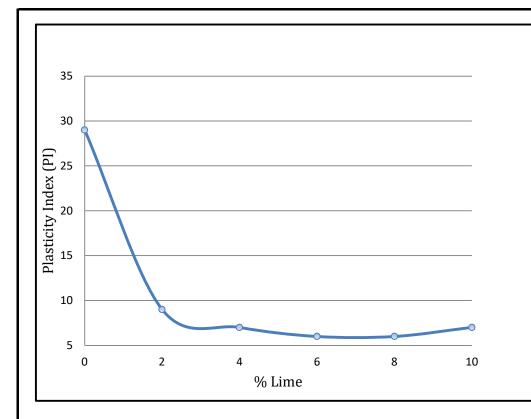
Atterberg Limits: LL = 45, PL = 24, PI = 21



ANN AUSTIN AND HUNTER CREEK SUBDIVISIONS WEIL ROAD

SANTA CLARA, GUADALUPE COUNTY, TEXAS

Drawn By: RB
Checked By: TA
Proj No: 00240902004.00
File Name



% Lime	<u>Plasticity</u>	<u>pH</u>	<u>LL</u>	<u>PL</u>
0	29	7.84	59	30
2	9	11.53	37	28
4	7	12.08	33	26
6	6	12.34	34	28
8	6	12.44	33	27
10	7	12.50	35	28

Test Location: CBR Sample No. 1

Material: Dark Brown Fat Clay (CH)

Test Method: TxDOT Item 260, Lime Treatment

Test Method: ASTM C 977, Appendix XI; pH:Lime Saturation Content

CBR Sample Location: 29.6070°, -98.1856°

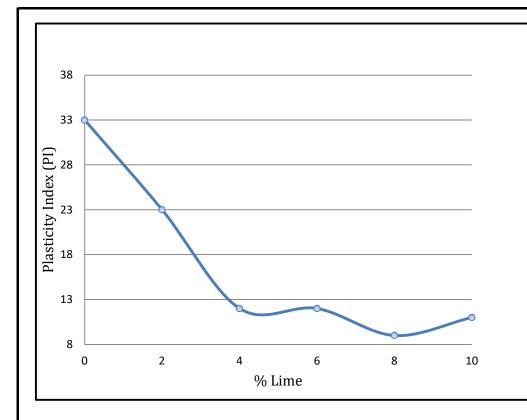


ANN AUSTIN AND HUNTER CREEK SUBDIVISIONS WEIL ROAD

SANTA CLARA, GUADALUPE COUNTY, TEXAS

Drawn By: RB
Checked By: TA
Proj No: 00240902004.00
File Name

LIME SERIES



% Lime	<u>Plasticity</u>	<u>pH</u>	<u>LL</u>	<u>PL</u>
0	33	7.68	64	31
2	23	11.15	55	32
4	12	11.67	48	36
6	12	12.12	50	38
8	9	12.23	43	34
10	11	12.31	48	37

Test Location: CBR Sample No. 3

Material: Dark Brown Fat Clay (CH)

Test Method: TxDOT Item 260, Lime Treatment

Test Method: ASTM C 977, Appendix XI; pH:Lime Saturation Content

CBR Sample Location: 29.5992°, -98.1937°



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ANN AUSTIN AND HUNTER CREEK SUBDIVISIONS WEIL ROAD

SANTA CLARA, GUADALUPE COUNTY, TEXAS

Drawn By: RB
Checked By: TA
Proj No:00210900483.00
File Name

LIME SERIES

APPENDIX B REFERENCE MATERIALS

EXPLORATION PROCEDURES

General

Various drill equipment and procedures are used to obtain soil or rock specimens during geotechnical engineering exploration activities. The drill equipment typically consists of fuel powered machinery that is mounted on a flat-bed truck or an all-terrain vehicle. The ground surface conditions at the site generally determine the type of vehicle to use.

Borings can be drilled either dry or wet. The drilling technique depends on the type of subsurface materials (clays, sands, silts, gravels, rock) encountered and whether or not subsurface water is present during the drilling operations. Sometimes a combination of both techniques is implemented.

The dry method can generally be employed when subsurface water or granular soils are not present. The dry method generally consists of advancing the augers without the use of water or drilling fluids. Air can be employed as necessary to remove cuttings from the borehole or cool the drilling bits during some drilling applications. The wet rotary process is generally used when subsurface water, rock or granular soils are present. The wet rotary process utilizes water or drilling fluids to advance the augers, remove cuttings from the borehole, and cool the drilling bits during drilling.

Sampling

Various sampling devices are available to recover soil or rock specimens during the geotechnical exploration program. The type of sampling apparatus to employ depends on the subsurface materials (clays, sands, silts, gravels, rock) encountered and on their consistency or strength. Most commonly used samplers are Shelby tubes, split-spoons or split-barrels, and NX core barrels. Depending on the subsurface conditions, sampling apparatus such as the Pitcher barrel, Osterberg sampler, Dennison barrel, or California sampler are sometimes used. The procedures for using and sampling subsurface materials with most of these samplers are described in detail by the American Society for Testing and Materials (ASTM). Sampling is generally performed on a 2-foot continuous interval to a depth of about 10 feet, followed by 5-foot intervals between the depths of about 10 to 50 feet, and on 10-foot intervals thereafter to the termination depth of the borings. However, sampling intervals may change depending on the project scope and actual subsurface conditions encountered.

If cohesive soils (clays and some silts) are present during drilling, samples are retrieved by using the Shelby tube sampler (ASTM D 1587) or the split-barrel sampler (ASTM D 1586). The Shelby tube is used to recover "virtually" undisturbed soil specimens that can be returned to the laboratory for strength and compressibility testing. The Shelby tube is a 3-inch nominal diameter, thin-walled tube that is advanced hydraulically into the soil by a single stroke of the drill equipment. The split-



barrel sampler is used when performing the Standard Penetration Test (SPT). The recovered sample is considered to be a "disturbed" specimen due to the SPT procedure. The split-barrel is advanced into the soil by driving the sampler with blows from a 140-pound hammer free falling 30 inches. The SPT procedure is performed to evaluate the strength or competency of the material being sampled. This evaluation is based on the material sampled, depth of the sample, and the number of blows required to obtain full penetration of the split-barrel sampler. This blow count or penetration resistance is referred to as the "N" value.

The split-barrel is typically used when cohesionless soils (sands, silts, gravels) are encountered or when good quality cohesive soils cannot be recovered with the Shelby tube sampler. The SPT procedure can be employed when rock or cemented zones are encountered. However, the split-barrel may not penetrate the rock or cemented zone if the layer is extremely hard, thus resulting in no sample recovery.

When rock or cemented zones are present and depending on the type of project and engineering testing required, rock coring may be implemented to recover specimens of the particular layer. Typically, an NX double tube core barrel (ASTM D 2113) is used.

Logging

During the drilling activities, one of our geologists or engineering technicians is present to make sure that the appropriate sampling techniques are employed and to extrude or remove all materials from the samplers. The samples are then visually classified by our field representative who records the information on a field boring log. Our field representative may perform pocket penetrometer, hand torvane, or field vane tests on the subsurface materials recovered from the Shelby tube samplers. If the SPT procedure is employed, our field representative will record the N values or blow counts that are germane to that particular field test. If rock coring is utilized, our field representative will calculate the percent recovery and Rock Quality Designation (RQD). The test data for all the field tests will be noted on the appropriate field boring log. Upon completion of the logging activities and field testing of the recovered soil or rock samples, representative portions of the specimens were placed in appropriately wrapped and sealed containers to preserve their natural moisture condition and to minimize disturbance during handling and transporting to our laboratory for additional testing.

When subsurface water is observed during the drilling and sampling operations, drilling will be temporarily delayed so the subsurface water level can be monitored for a period of at least 15 to 30 minutes. Depending on the rise of the subsurface water in the borehole and project requirements, subsurface water measurements may be monitored for periods of 24 hours or more. Generally, observation wells or piezometers are installed in the completed boreholes to monitor subsurface water levels for periods longer than 24 hours.

Following completion of drilling, sampling, and subsurface water monitoring, all boreholes are backfilled with soil cuttings from the completed borings unless the client requests or local



ordinance requires special backfilling requirements. If there are not enough soil cuttings available, clean sand will be used to backfill the completed boreholes.

Details concerning the subsurface conditions are provided on each individual boring log presented in Appendix A. The terms and symbols used on each boring log are defined in the Legend Sheet which is also presented in Appendix A.

LABORATORY TESTING PROCEDURES

Classification and Index Testing

The recovered soil samples were classified in the laboratory by a geoprofessional using the USCS as a guide. Samples were tested for the following properties in general accordance with the applicable ASTM standards:

- Moisture content (ASTM D2216)
- Atterberg Limits (ASTM D4318)
- Percent material passing the No. 200 sieve (ASTM D1140)
- Grain Size Analysis (ASTM D6913)
- California Bearing Ratio (ASTM D1883)
- Standard Proctor (ASTM D698)
- Lime Treatment of Clay Soil (TxDOT Item 260)
- Lime Saturation Content by pH (ASTM C977)
- Soluble Sulfates (ASTM C1580)

Results of tests for moisture content, Atterberg Limits, and percent material passing the No. 200 sieve are presented on individual boring logs in Appendix A. The results are also tabulated on the Summary of Laboratory Results sheet in Appendix A.

